

ASSESSMENT OF OPTICAL BASED CONTROL METHODS FOR THERMO-MECHANICAL FATIGUE

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° Rolls-Royce plc, Derby, DE24 8BJ



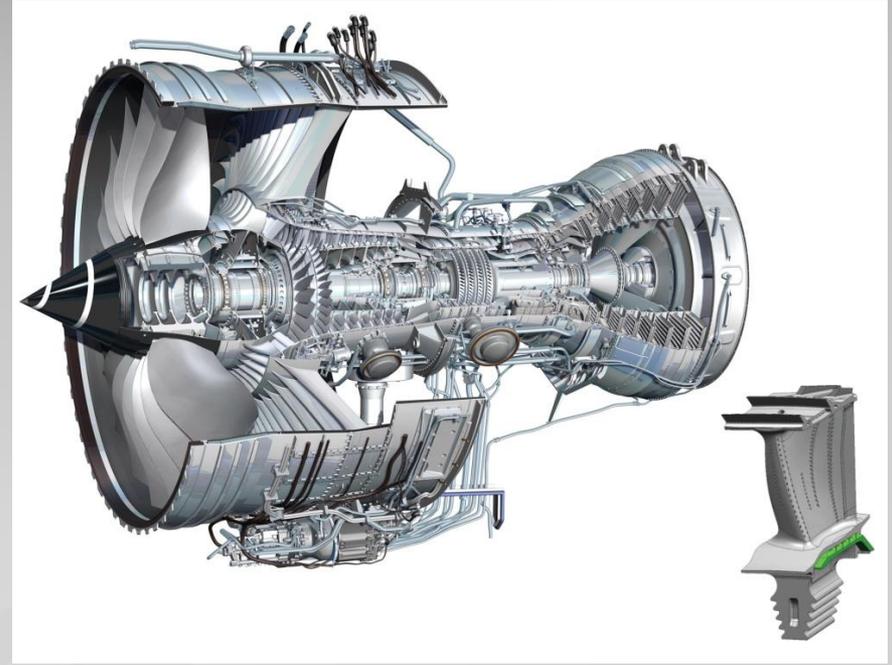
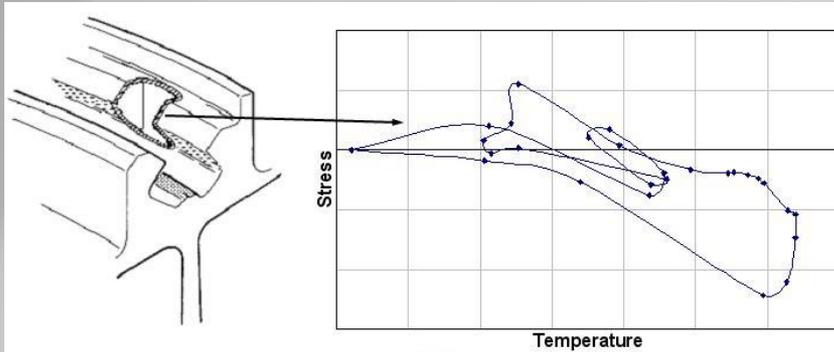
Prifysgol Abertawe
Swansea University



Rolls-Royce[®]

Industrial Motivation

- Increased turbine entry temperatures
- Thinner disc rims and advanced cooling systems leading to larger thermal gradients
- Complex loading regimes within the gas turbine leading to diverse phasing between temperature and strain



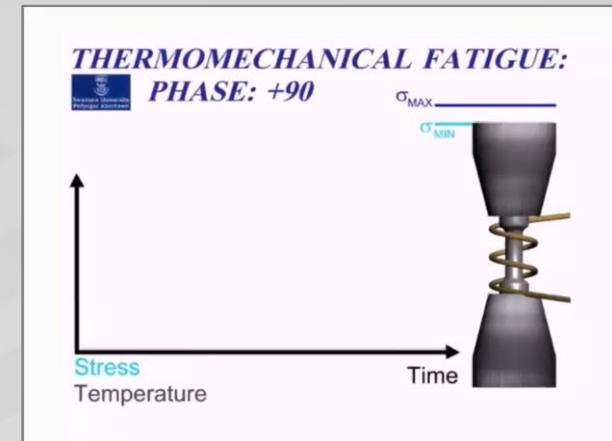
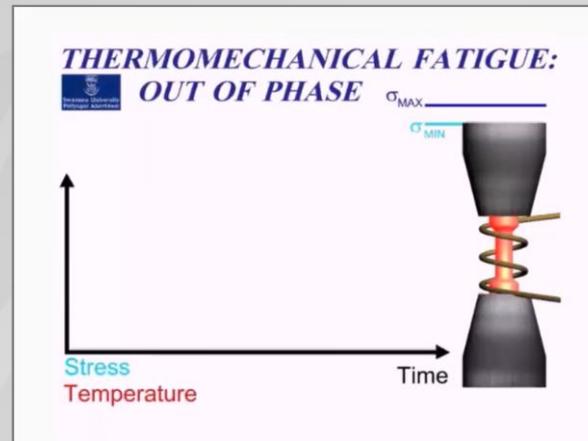
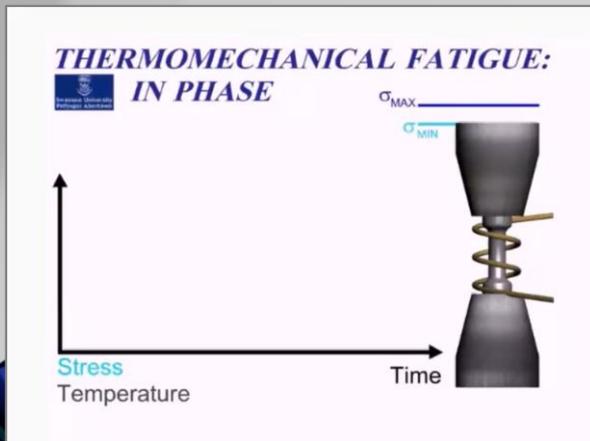
- Extrapolation of isothermal fatigue (IF) results to incorporate these effects show limited success
- Generation of TMF data is required to allow the development of lifing methodologies under TMF loading

Thermo-Mechanical Fatigue (TMF)

- Diverse mechanisms are involved, Primarily . . .

Fatigue Creep Oxidation

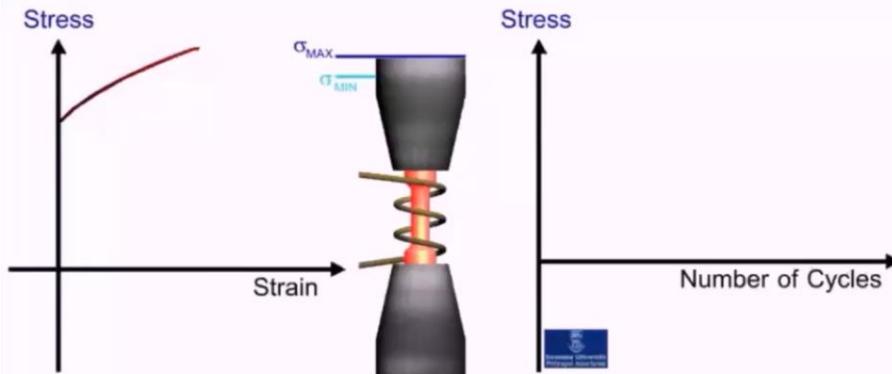
- TMF loading can be more damaging than isothermal fatigue at an equivalent T_{\max}
- Complex interaction within diverse *phase angles* between peak temperature and strain range
- Resulting in strain R ratios varying between 0 and $-\infty$ depending on the phase angle, ϕ .



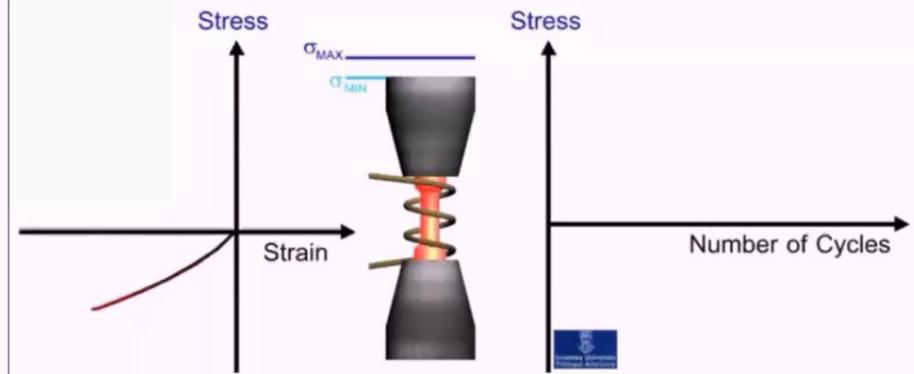
Typical TMF Hysteresis Behaviour

- Initial material behaviour may change significantly during the test.
- Understanding the stress/strain evolution throughout the test is often critical in order to be able to predict life.
- Cycle may evolve to very different stress conditions due to the interaction of plasticity and creep which often makes TMF tests differ significantly from isothermal fatigue.
- However without accurate temperature control, reliable test data for component lifing cannot be achieved.

In-Phase ($\phi = 0^\circ$)

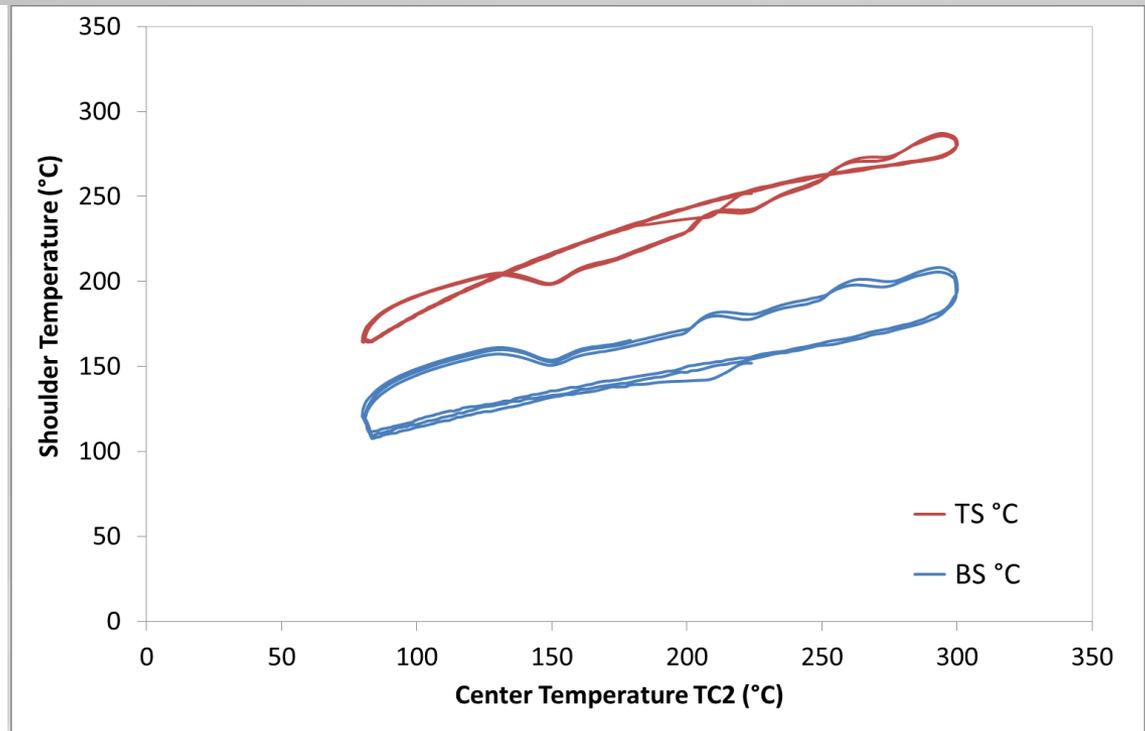
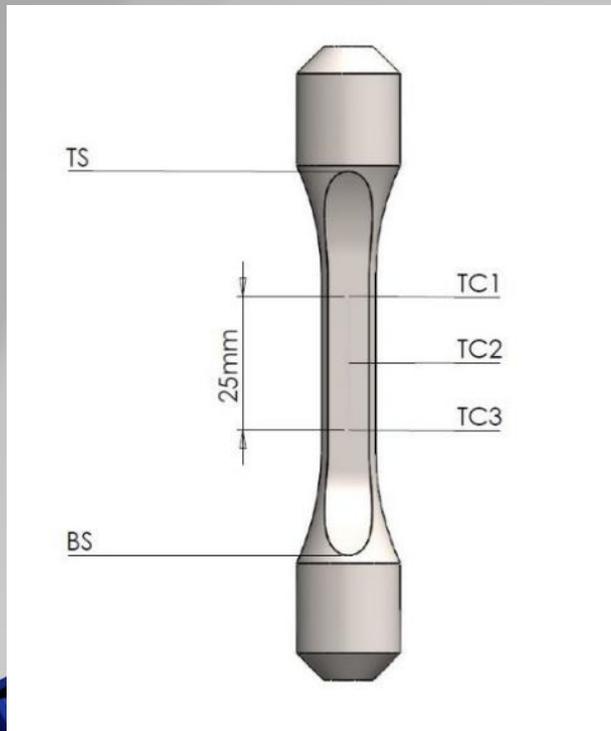


Out-Phase ($\phi = -180^\circ$)



Thermocouple Shoulder Control

- Unfavourable to weld on the specimen gauge length – Nucleation of cracks
- Contact temperature measurement can be achieved at the specimen shoulder.
- Complex setup and often temperatures at either shoulder are not stable with loops overlapping and drifting, unacceptable for temperature control purposes.

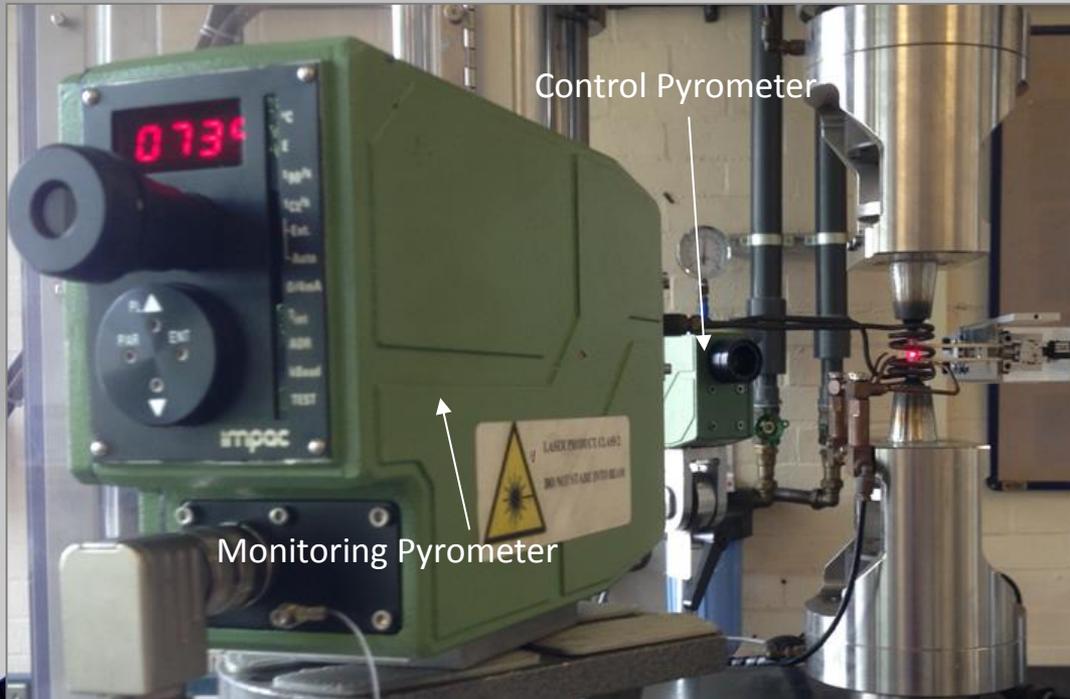


TMF Standards:

- **ASTM E2368-10:** Standard Practice for Strain Controlled Thermo-mechanical Fatigue Testing (*Released in 2004, updated in 2010*)
- **ISO 12111:2011:** Metallic materials – Fatigue Testing – Strain Controlled Thermo-mechanical Fatigue Testing Method (*Released 2011*)

Pyrometer Control

- Non-invasive temperature control can be achieved using pyrometry
- High temperature pre-exposure to produce a constant surface emissivity, ϵ .



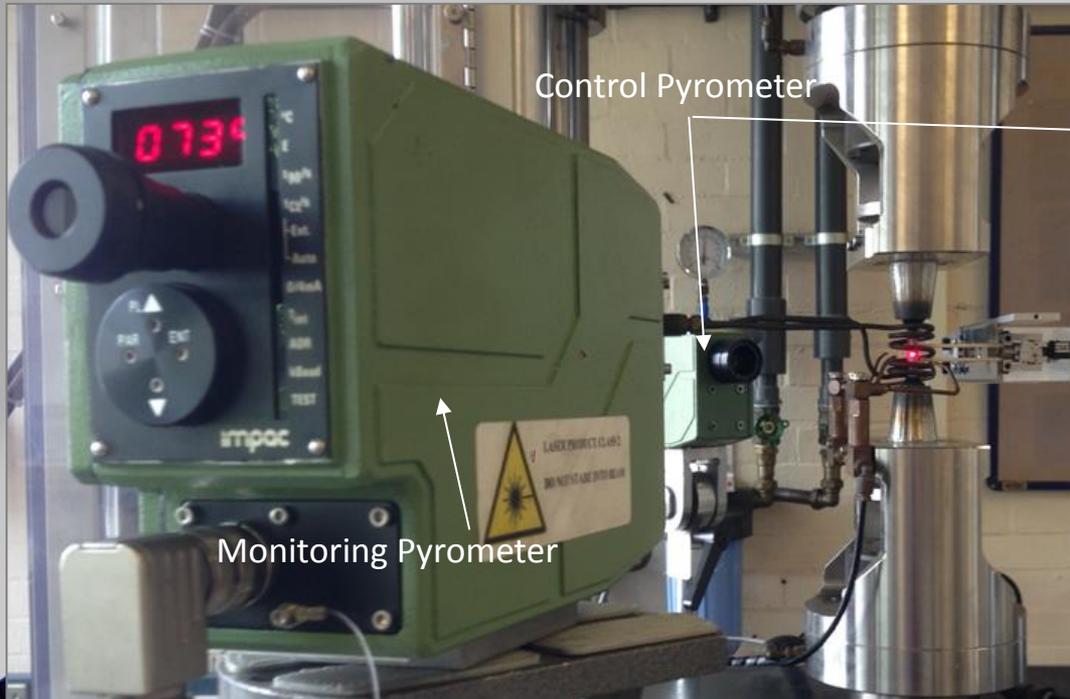
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Pyrometer Control

- High temperature pre-exposure can reduce Fatigue life
Encinas-Oropesa, A., Drew, G. L., Hardy, M. C., Leggett, A. J., Nicholls, J. R., and Simms N. J., Proceedings of the Eleventh TMS International Symposium, Superalloys, pp. 609-618, 2008
- Thermal Profiling still achieved using thermocouples

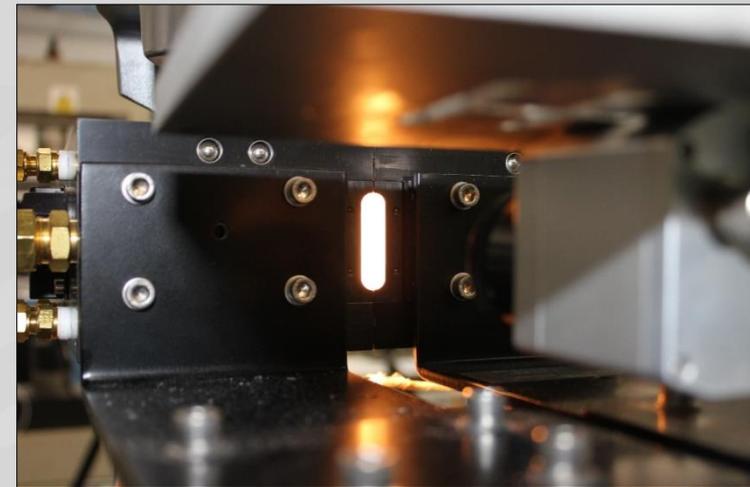
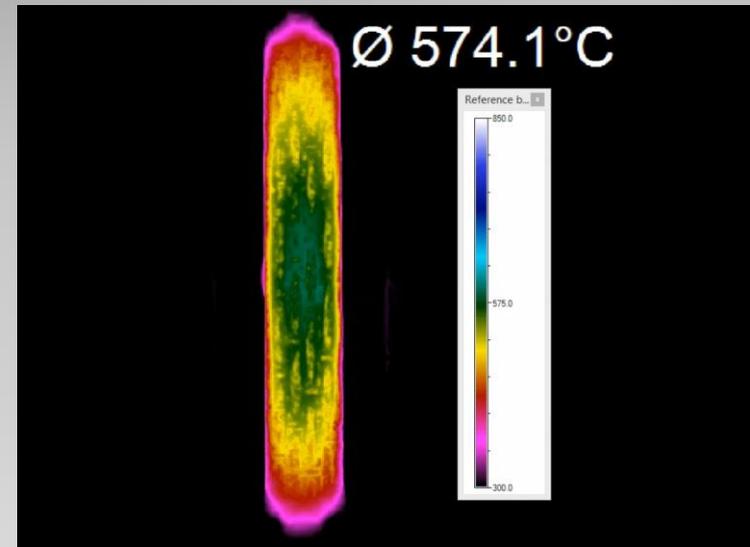


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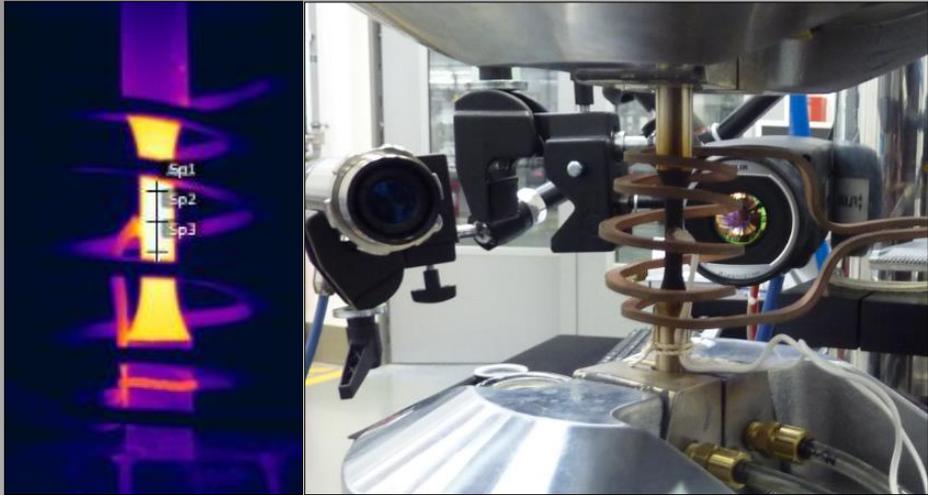
Introduction - Thermography

- Technique that can deliver....
 - Accurate Temperature control
 - Incorporates Thermal Profiling
 - Not influenced by Surface emissivity
 - Completely Non-Invasive
 - Metallic and non-metallic materials
 - Robust and repeatable
- Infra-red, Thermography?

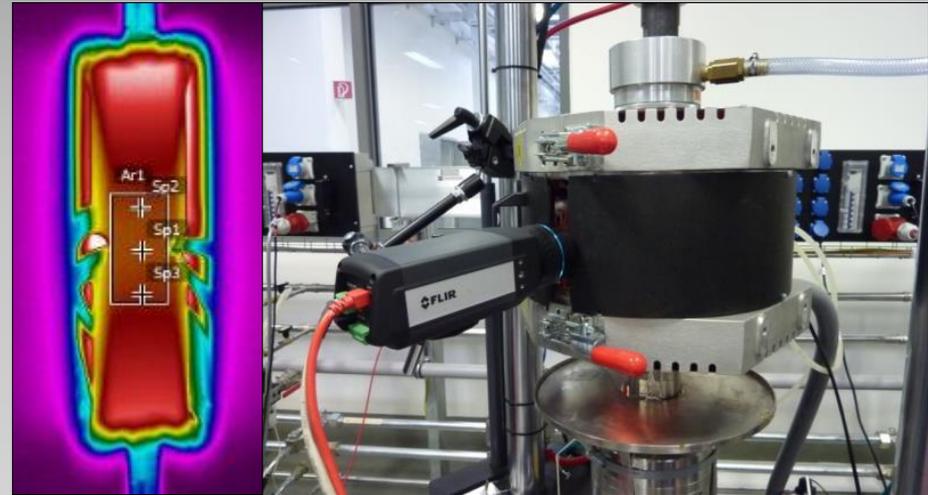


Previous Work – Rolls-Royce plc, MTOC, Germany

Induction Heating



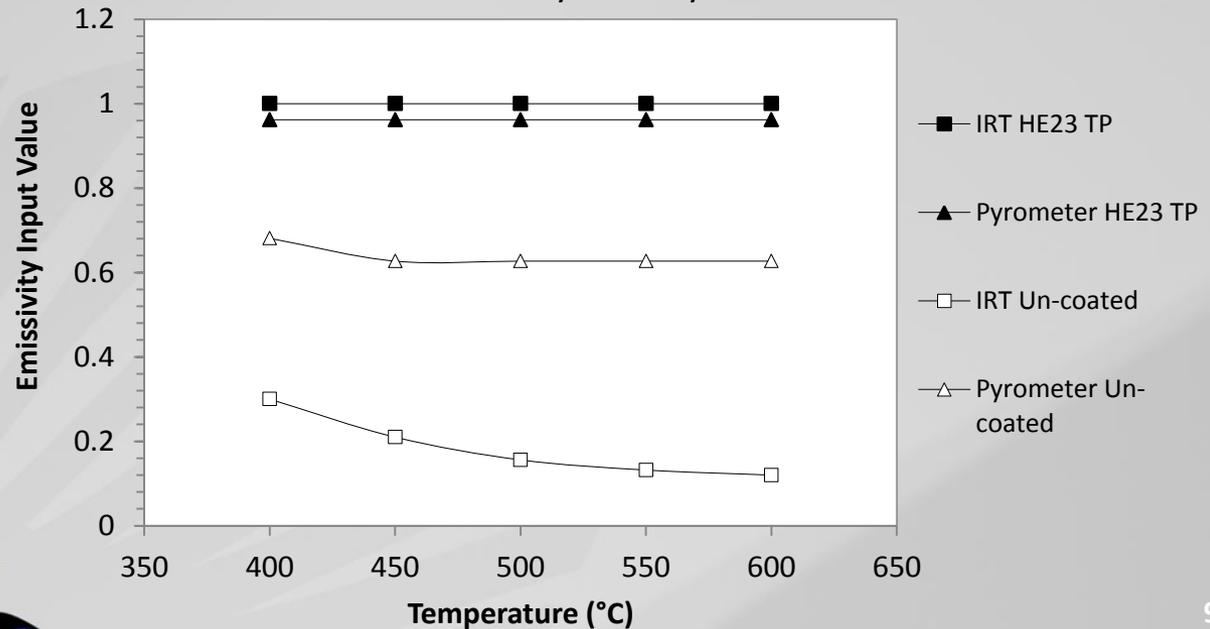
Radiant Lamp Furnace Heating



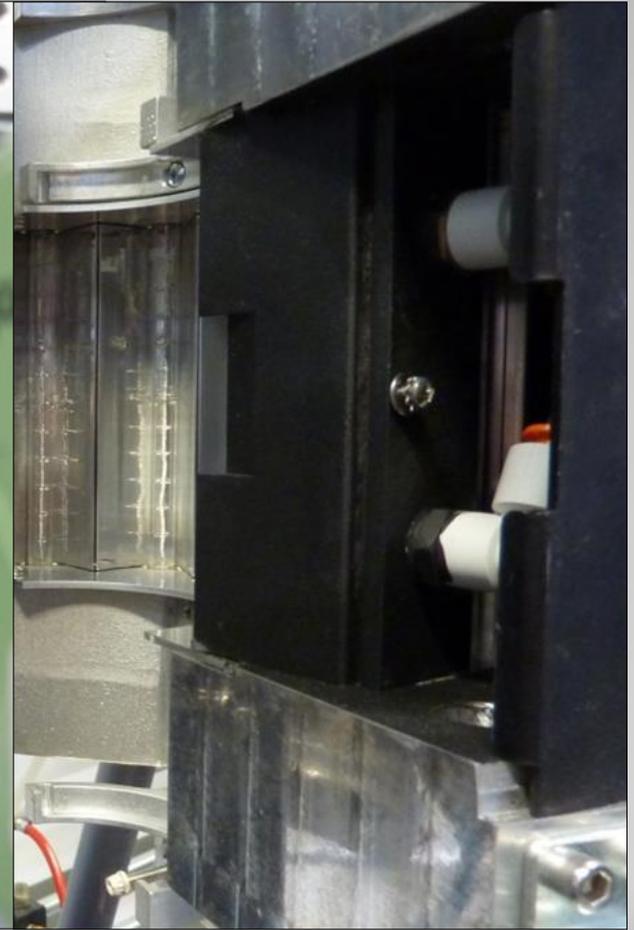
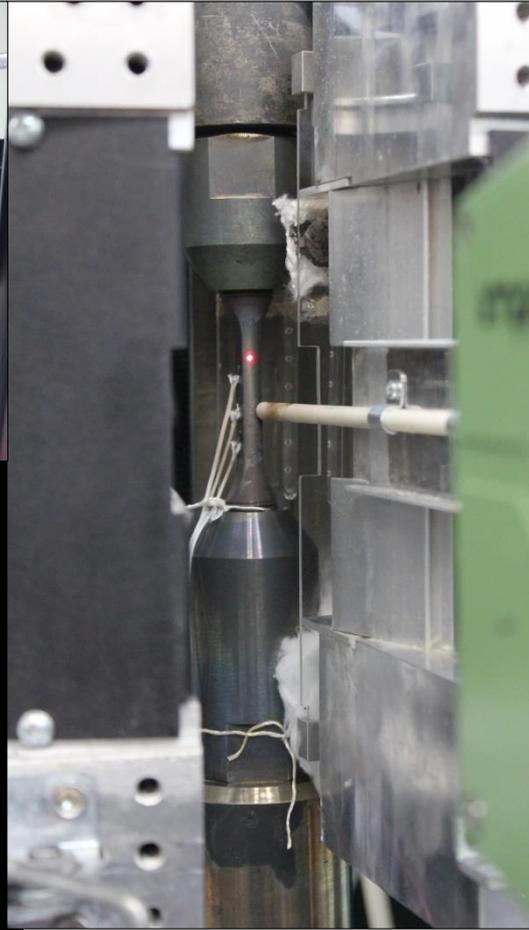
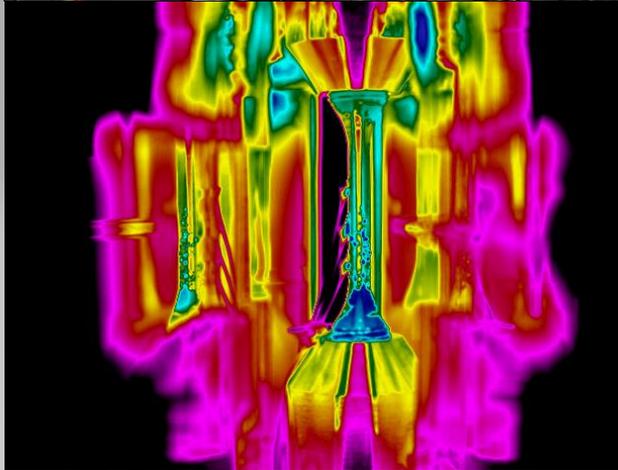
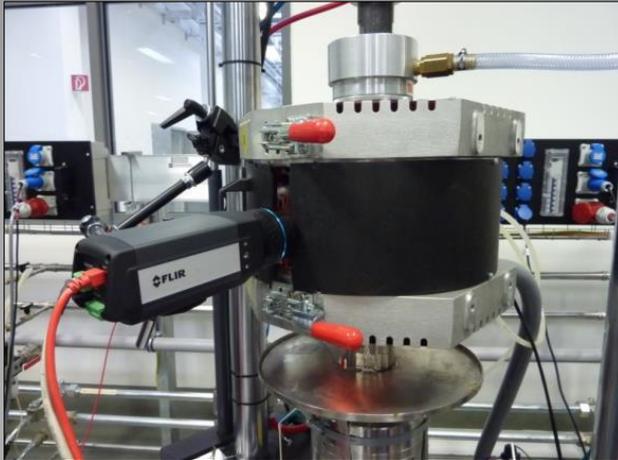
HE23 Thermal Paint



Surface Emissivity Stability



Previous Work – Radiation Reflections



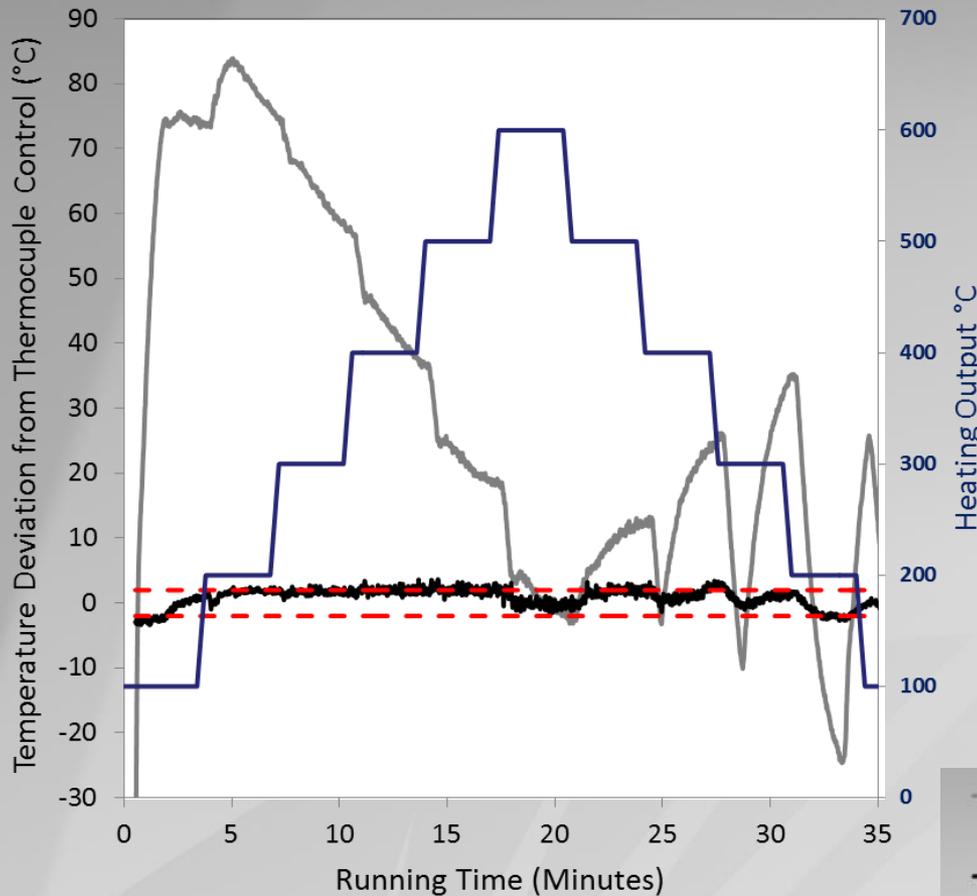
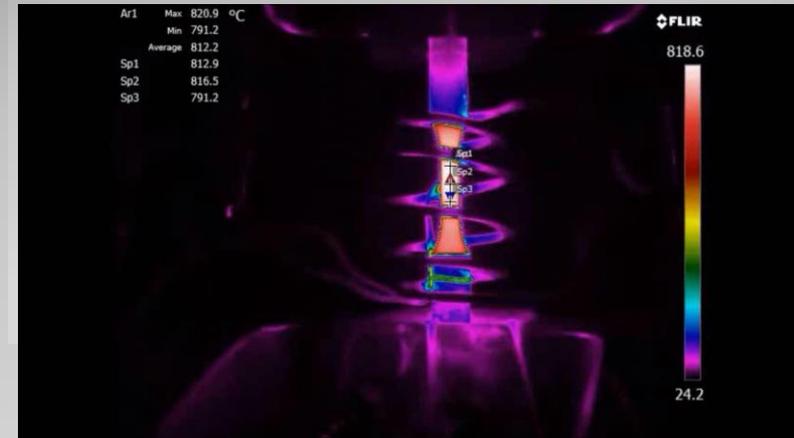
3-5 July 2017 – Fatigue
2017, Downing College,
Cambridge, UK

Jones, J.P., et al., Non-invasive temperature measurement and control techniques under thermomechanical fatigue loading. *Materials Science and Technology* **2014**. 30(15): p. 1862-1876

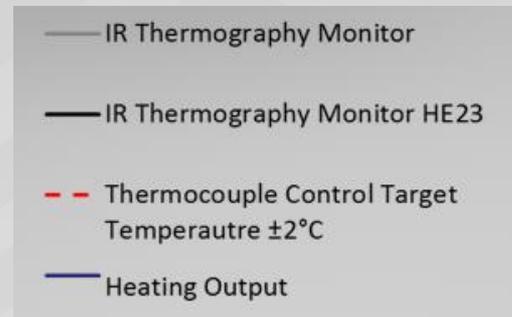
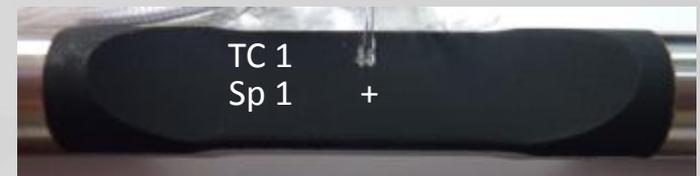
Jones, J.P., et al. Assessment of Infrared Thermography for Cyclic High-Temperature Measurement and Control. in 4th Evaluation of Existing and New Sensor Technologies for Fatigue, Fracture and Mechanical Testing. **2015**. Toronto: ASTM International.

Previous Work – HE23 Stability

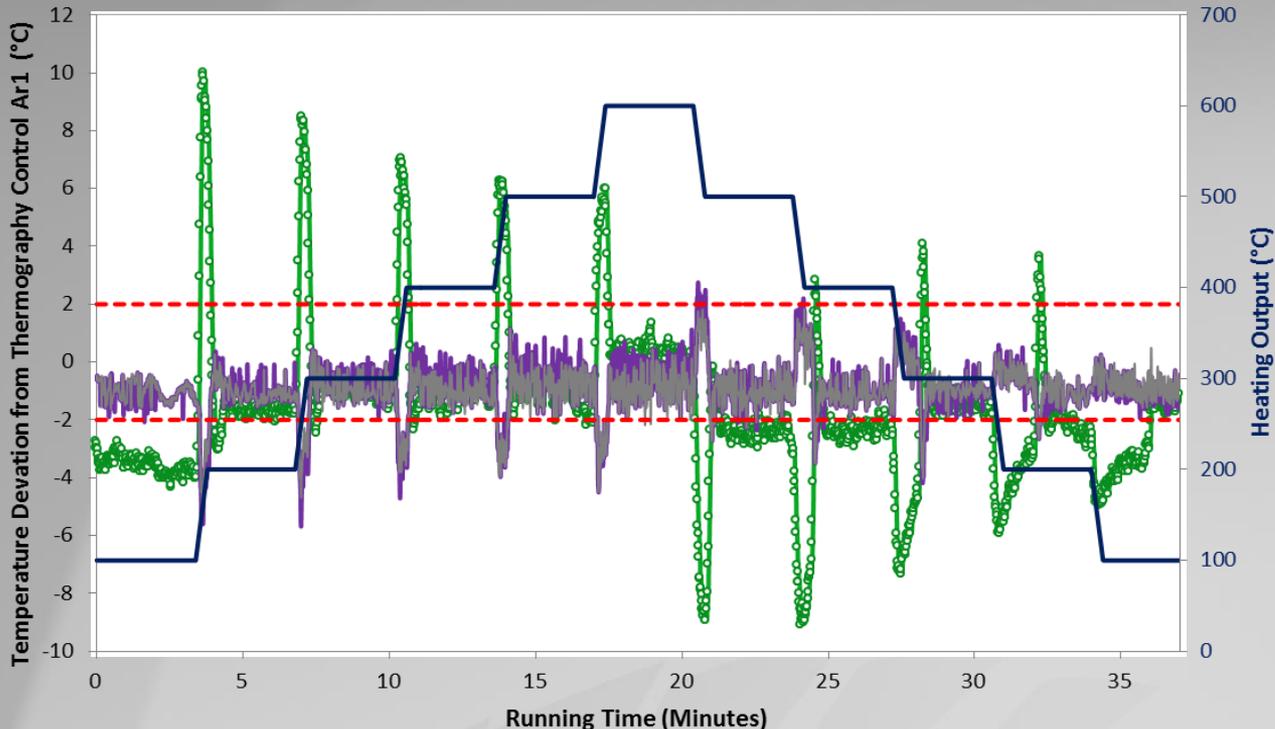
Thermography View



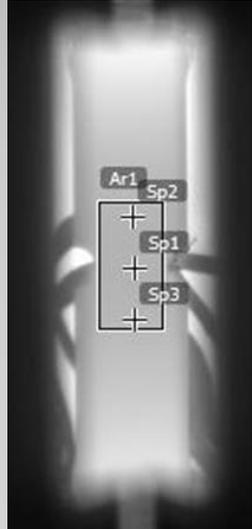
HE23 Coated Test Piece



Previous Work – Thermography vs Thermocouples



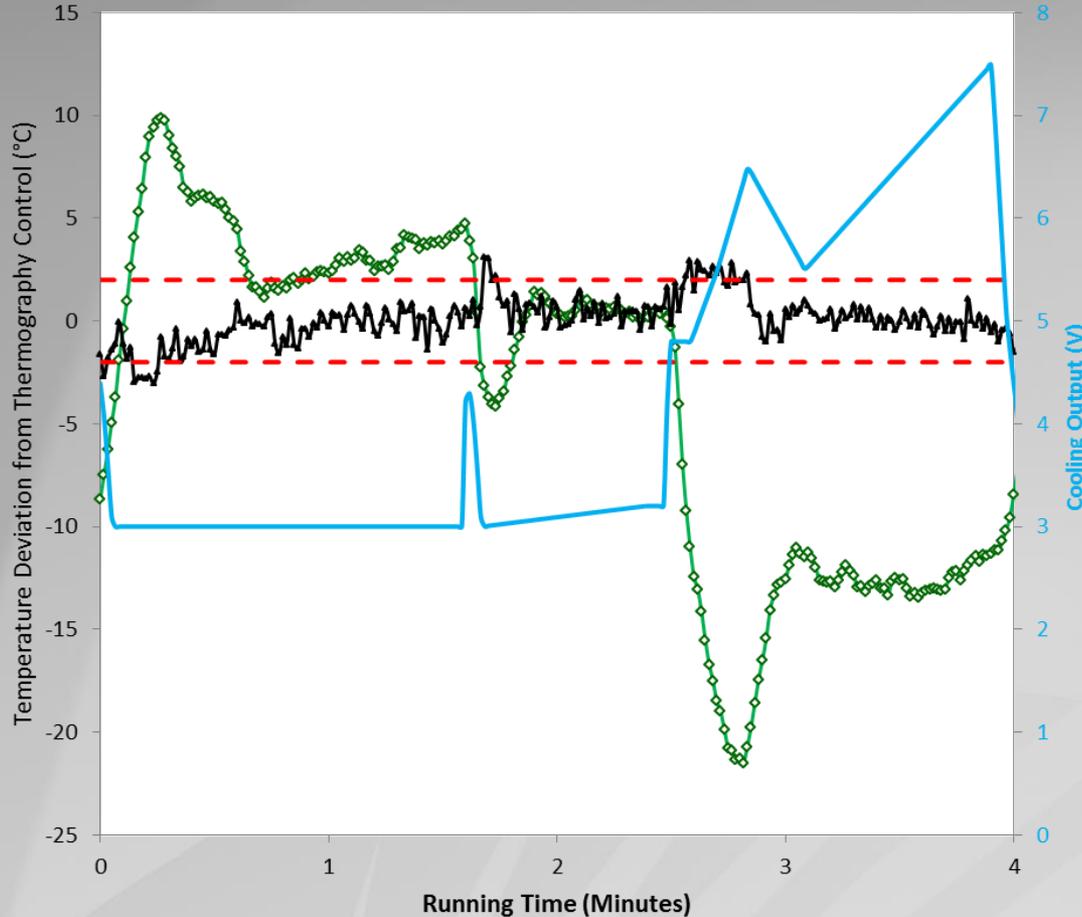
Thermography View



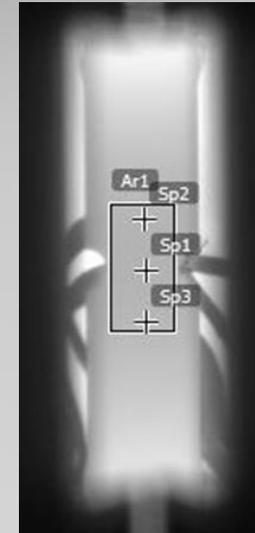
- Thermocouple Monitor T1
- IR Thermography Monitor Ar1 (Post test analysis)
- Heating Output
- IR Thermography Monitor Sp1 (Post test analysis)
- - - IR Thermography Control Target Temperature $\pm 2^{\circ}\text{C}$

- Jones, J.P., et al., Non-invasive temperature measurement and control techniques under thermomechanical fatigue loading. *Materials Science and Technology* **2014**. 30(15): p. 1862-1876
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Previous Work – Thermography vs Thermocouples



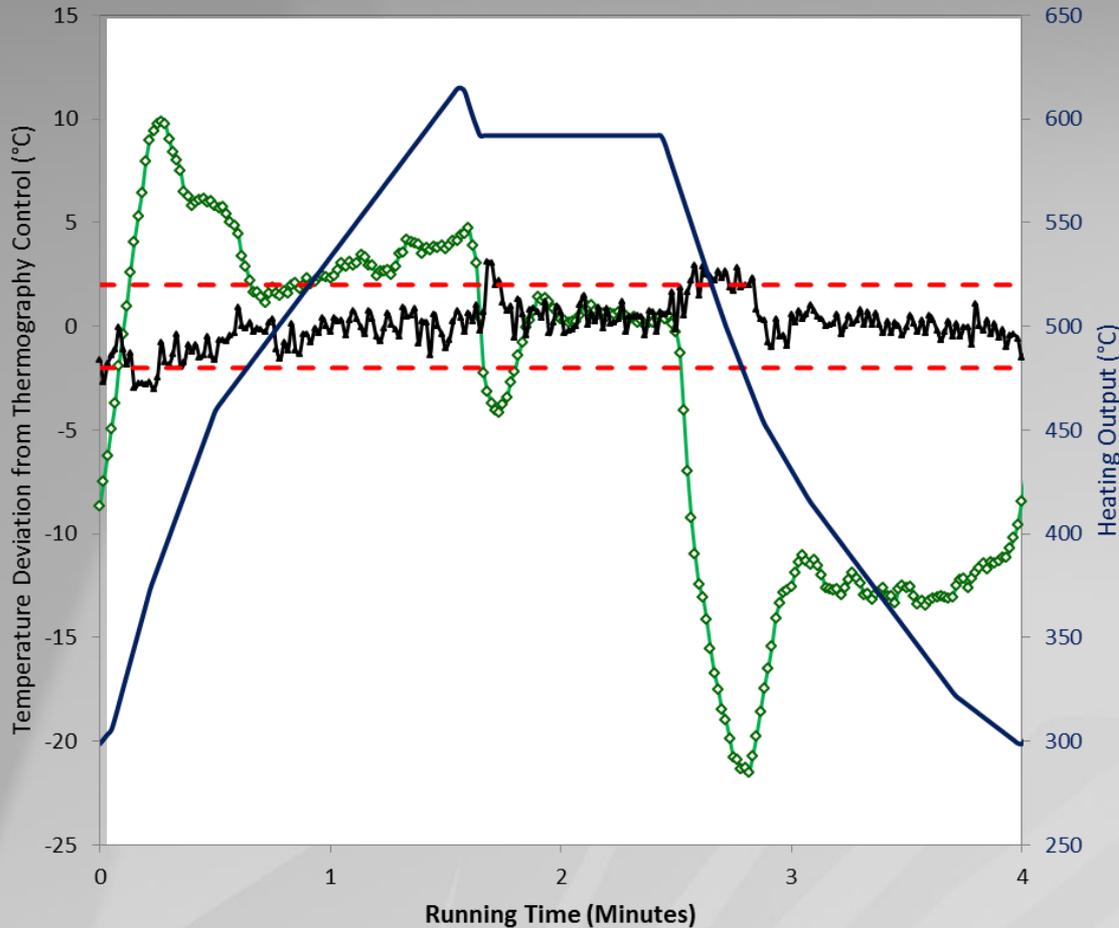
Thermography View



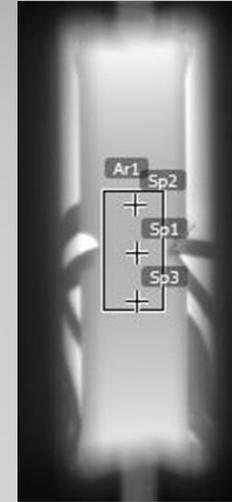
- ◇— Thermocouple Monitor TC1
- IR Thermography Monitor Sp1 (Post test analysis)
- - - IR Thermography Control Ar1 Target Temperature $\pm 2^{\circ}\text{C}$
- Cooling Output

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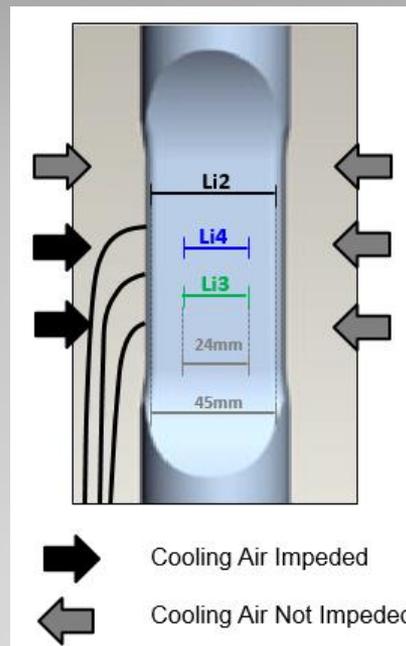
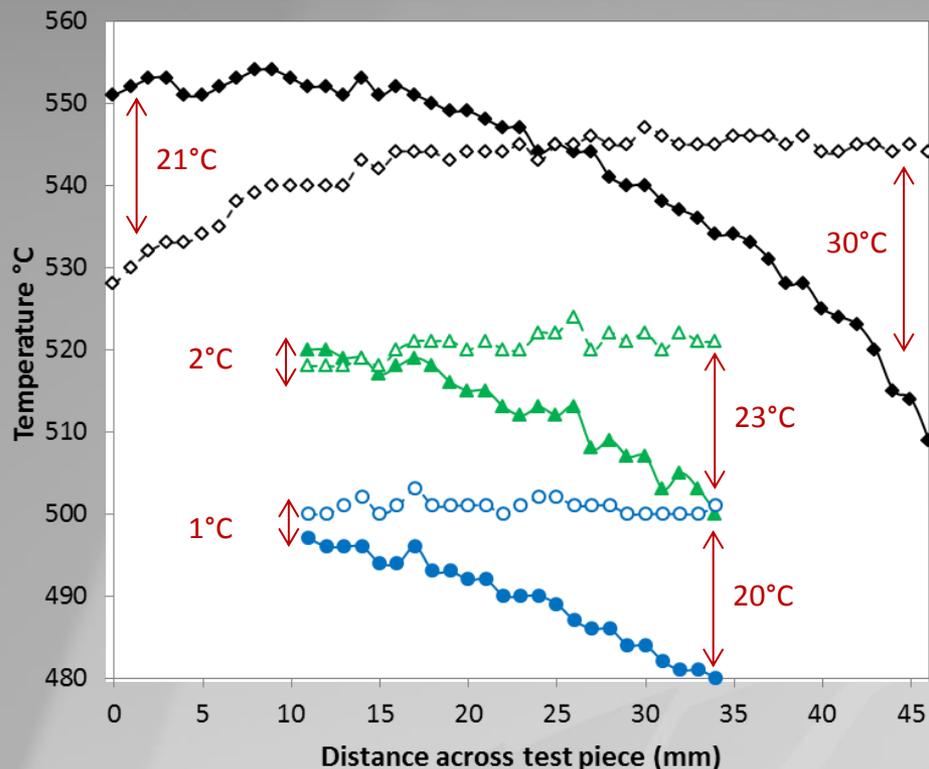
Thermography View



- ◇ Thermocouple Monitor TC1
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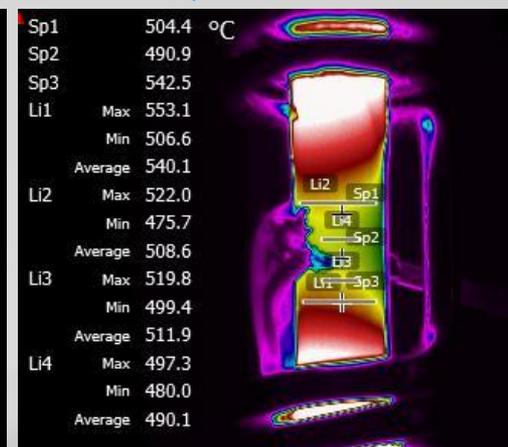
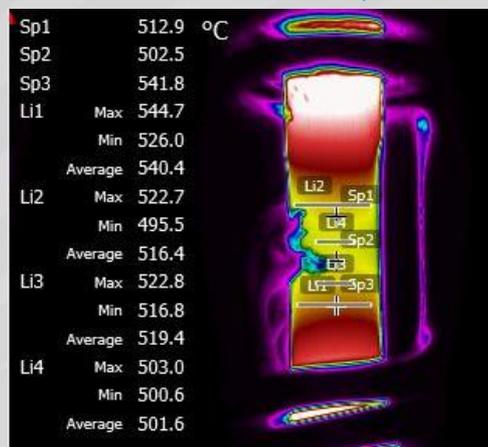
Previous Work – Thermocouple Shadowing



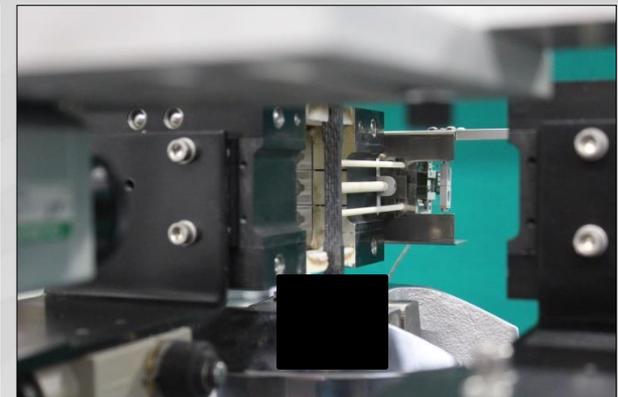
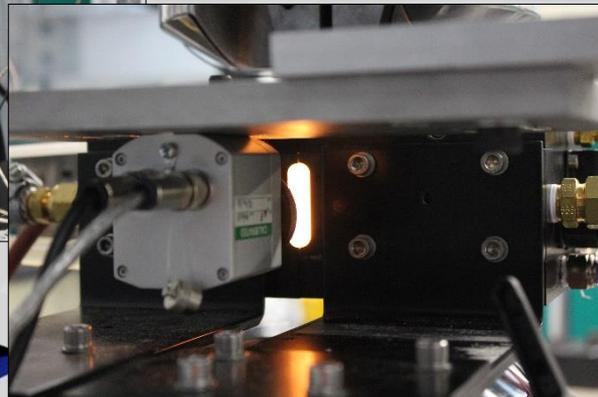
- Li1 Not Impeded
- ▲— Li3 Not Impeded
- Li4 Not Impeded
- -◇- - Li1 Air Impeded
- -△- - Li3 Air Impeded
- -○- - Li4 Air Impeded

Cooling Direction →

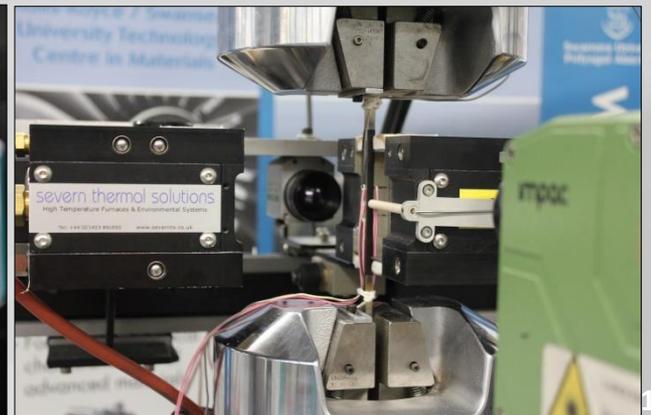
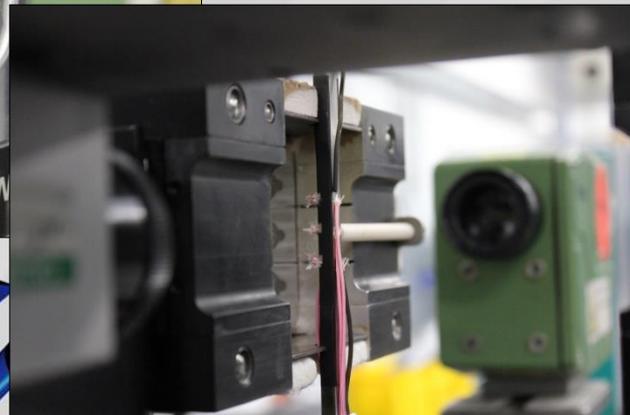
← Cooling Direction



Bespoke TMF Setup – Non Metallic Materials



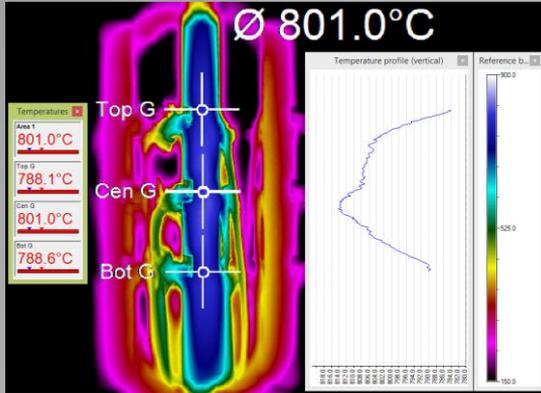
Bespoke TMF Setup – Non Metallic Materials



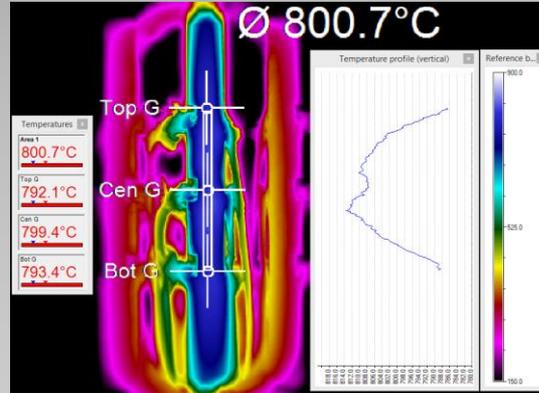
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Control Method Comparison

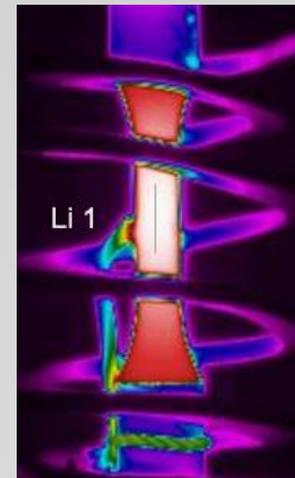
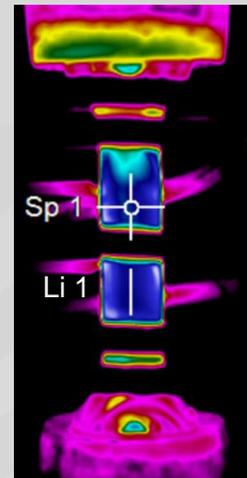
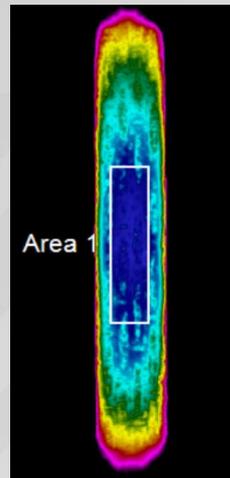
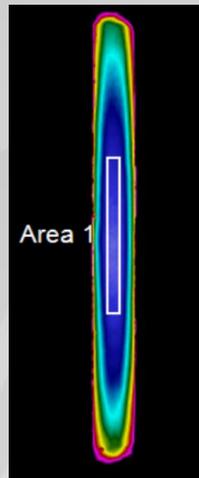
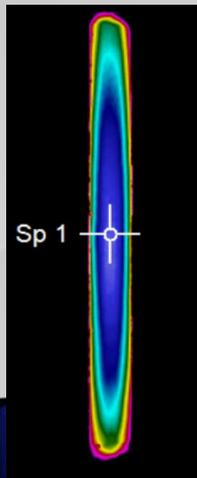
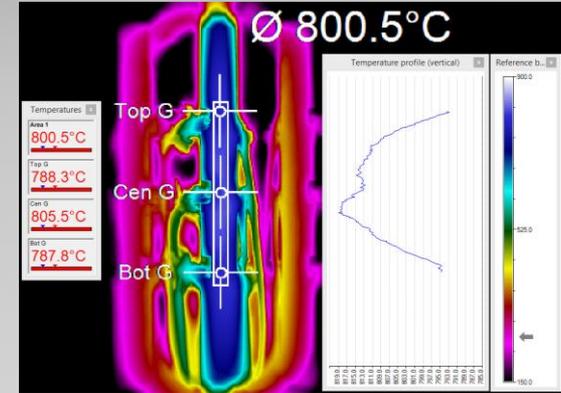
Single Point Control



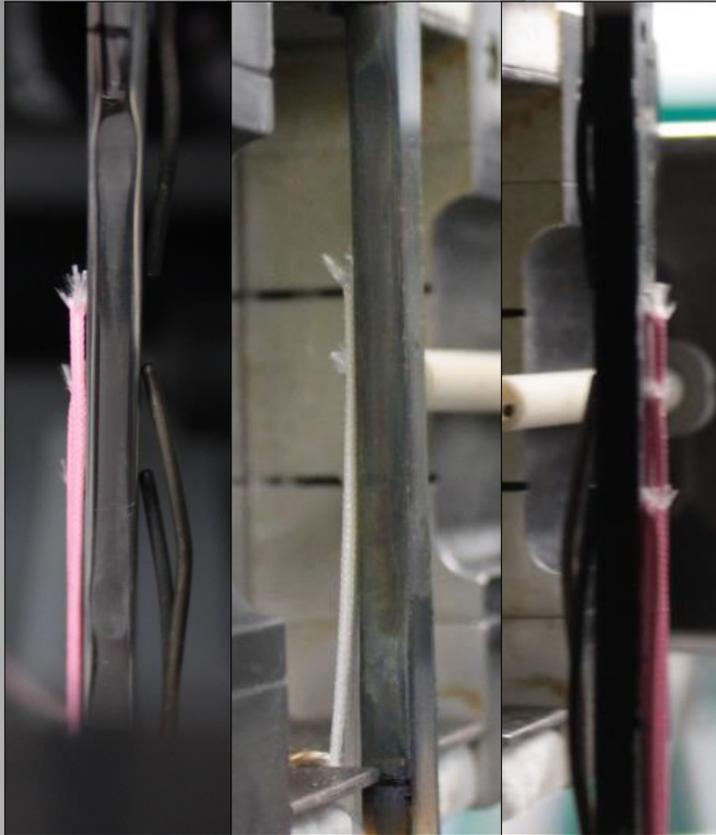
Small Area Control (2 x 25mm)



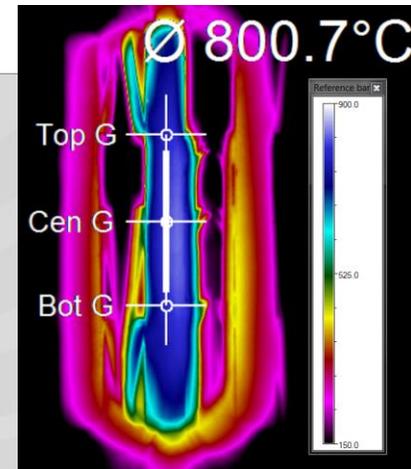
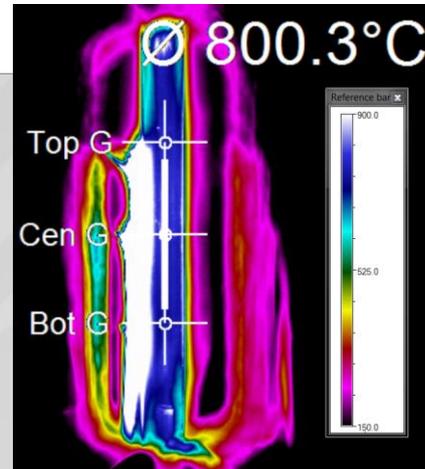
Large Area Control (3 x 30mm)



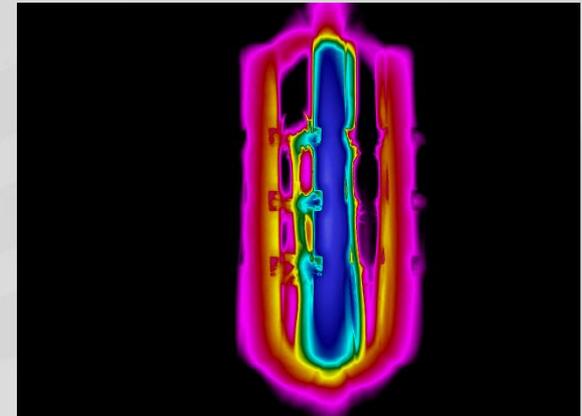
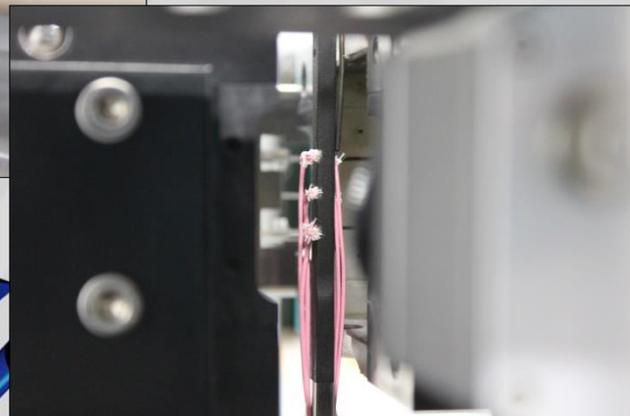
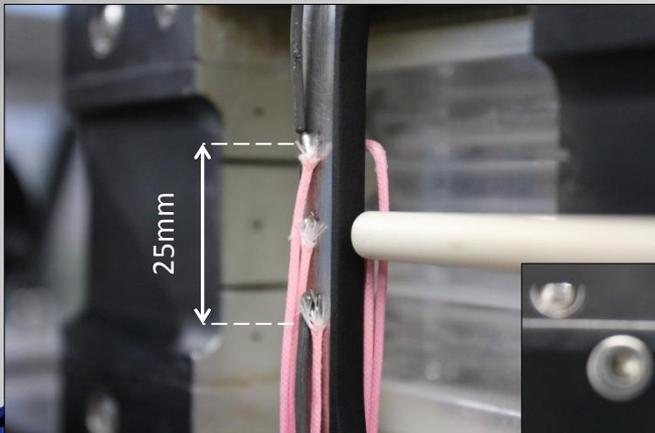
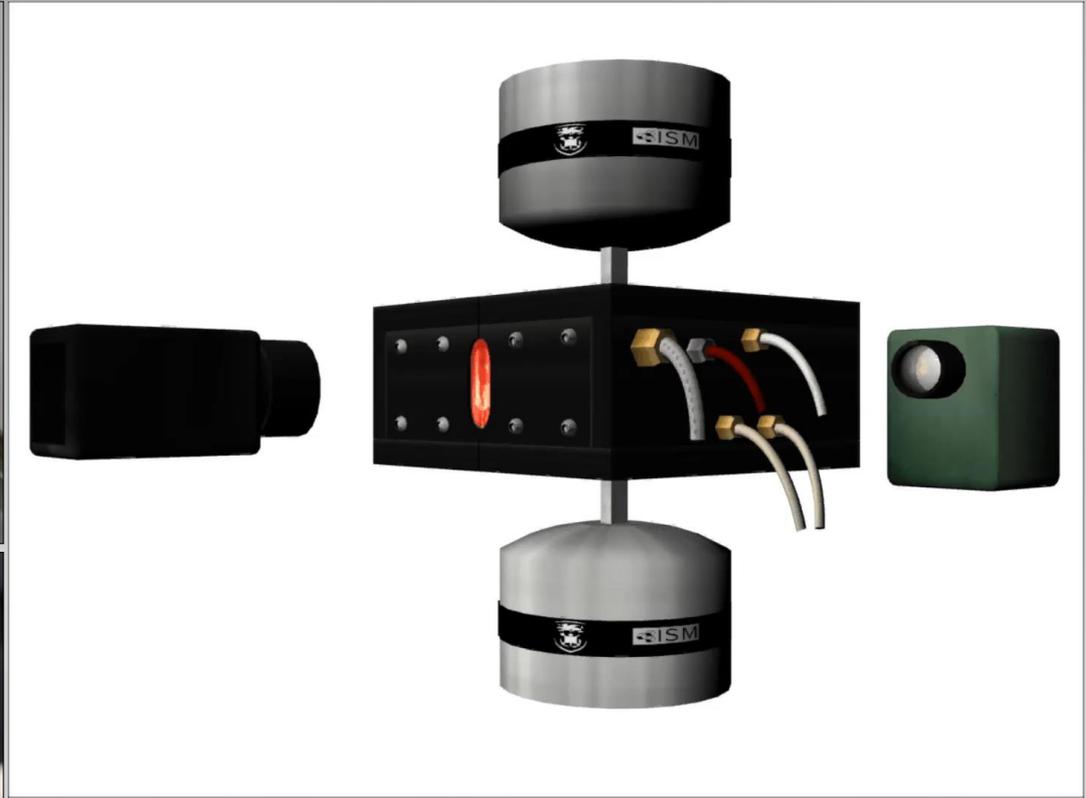
Diverse Surface Conditions



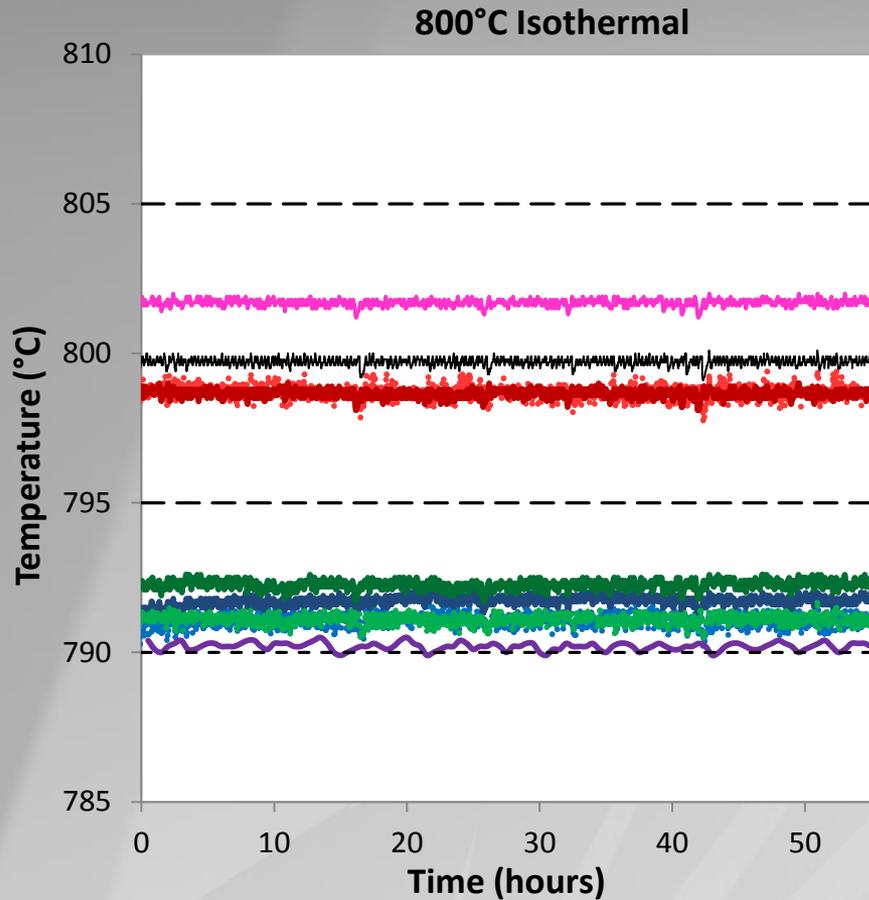
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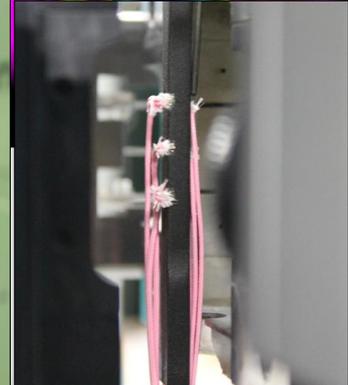
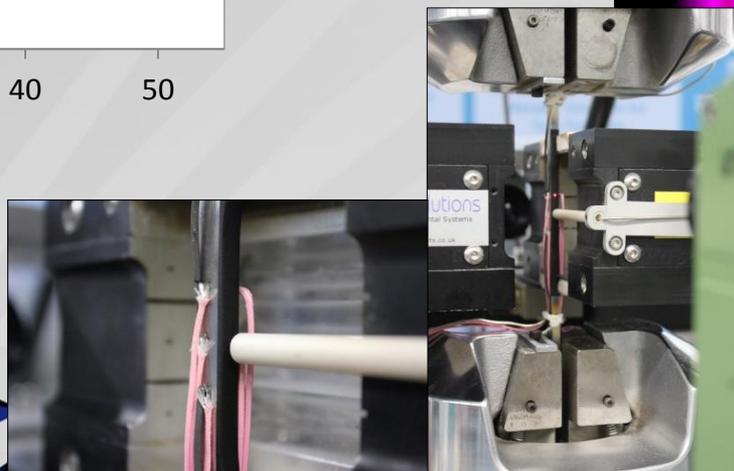
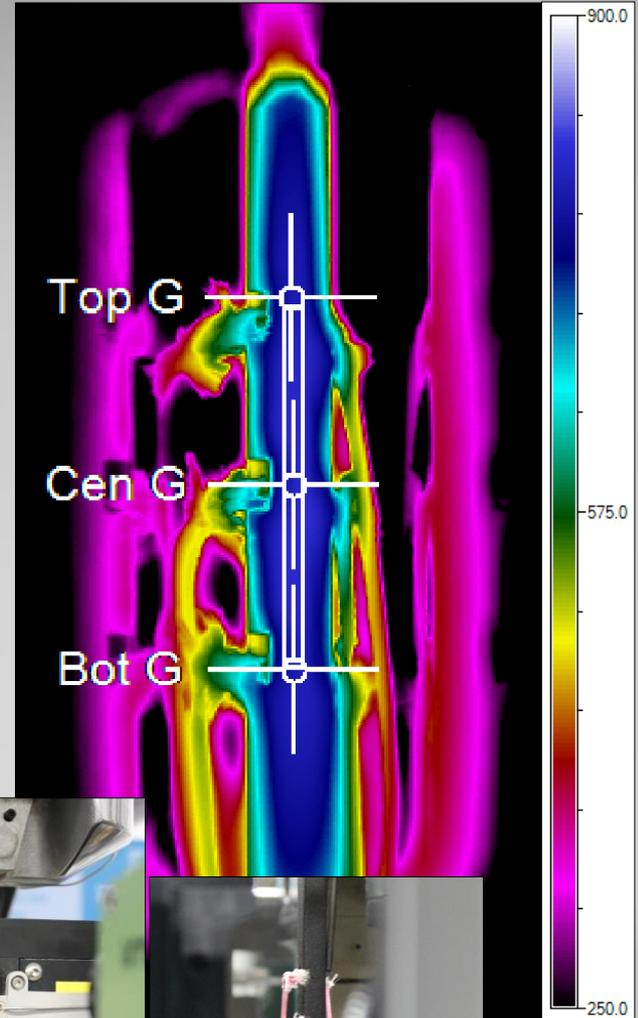
Temperature Measurement Comparisons



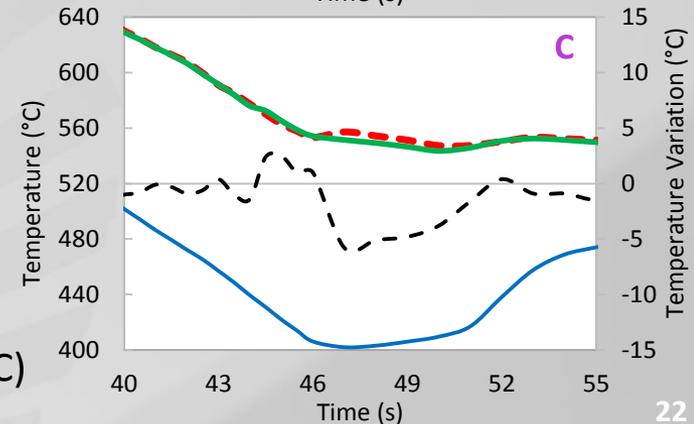
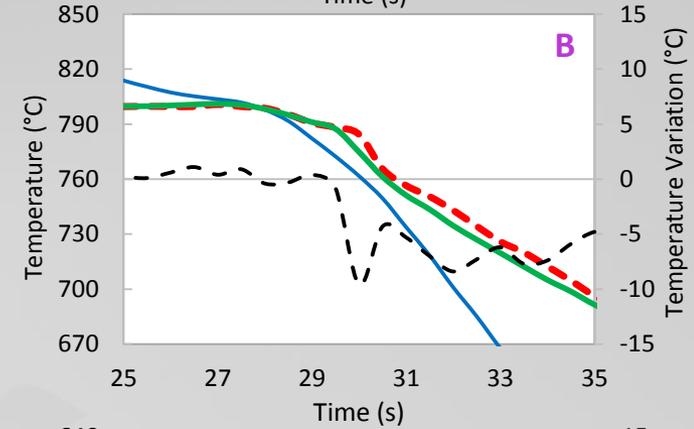
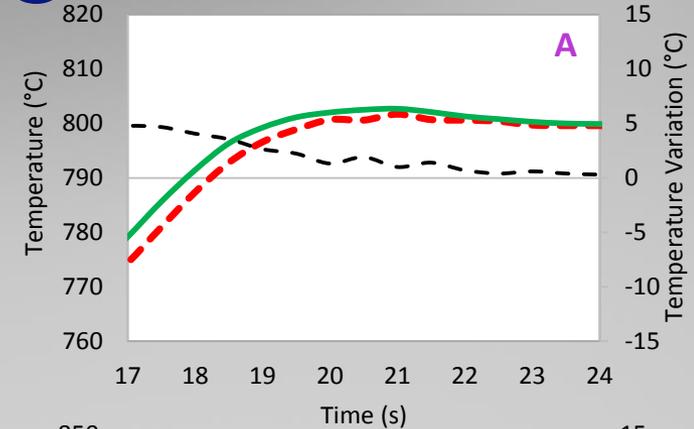
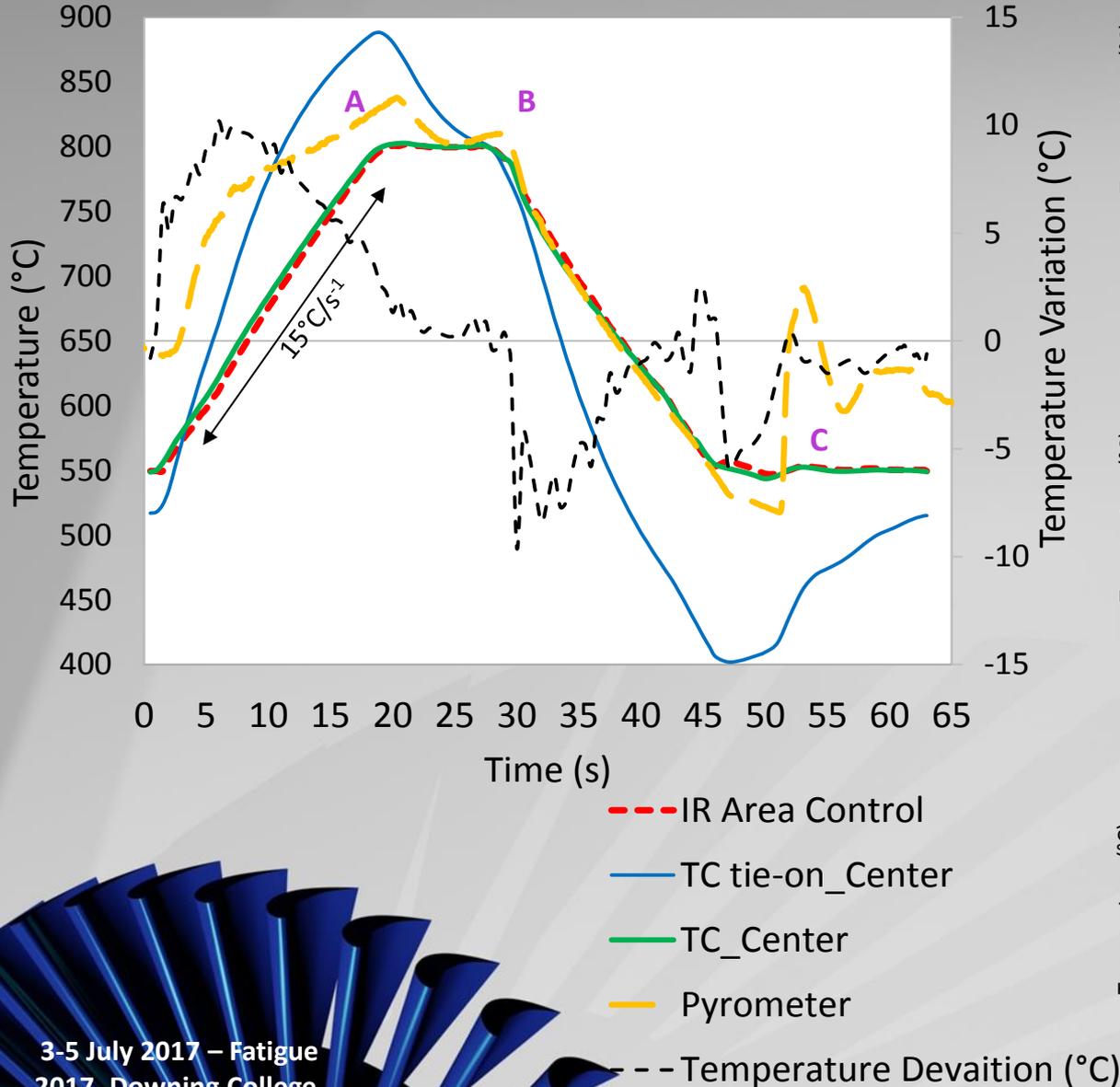
Isothermal Accuracy, IR vs TC



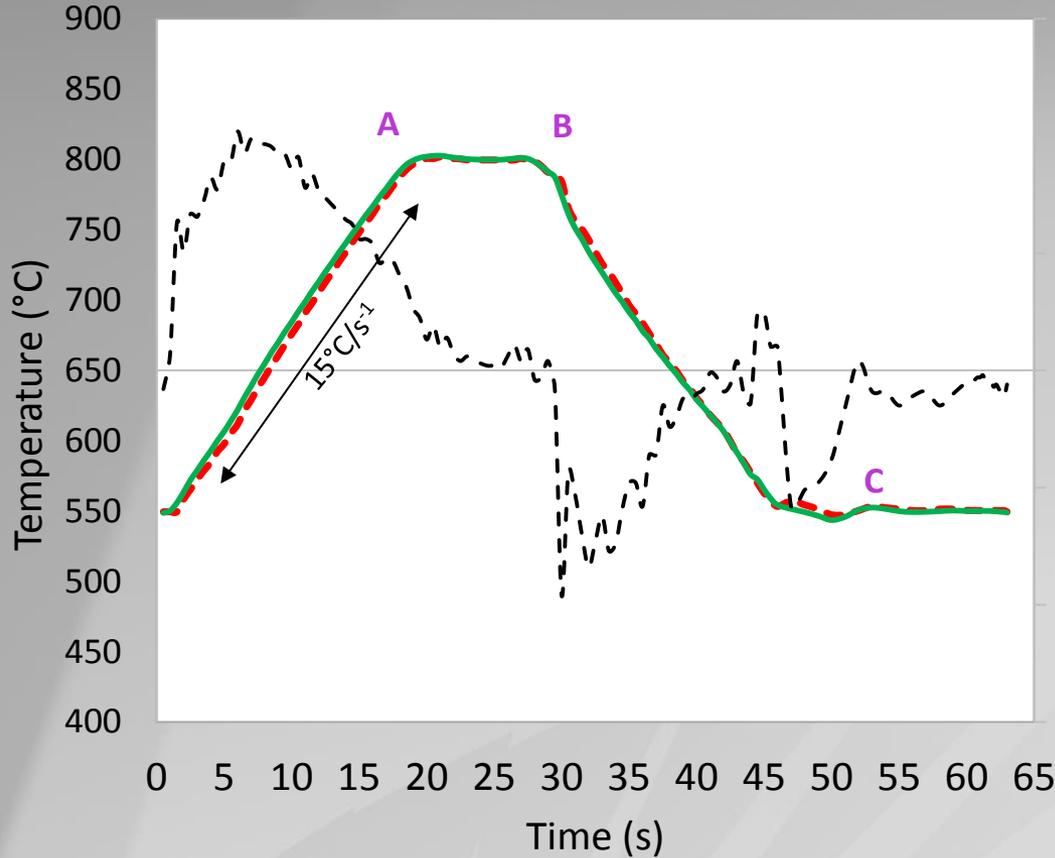
- IR_Area Control
- IR_Center
- TC_Center
- TC_Center Face
- IR_Top
- TC_Top
- Pyrometer_Top
- IR_Bottom
- TC_Bottom
- - ±5°C
- - - ±10°C



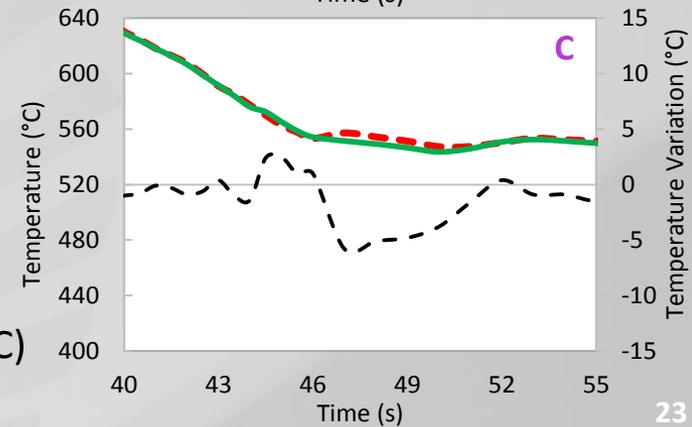
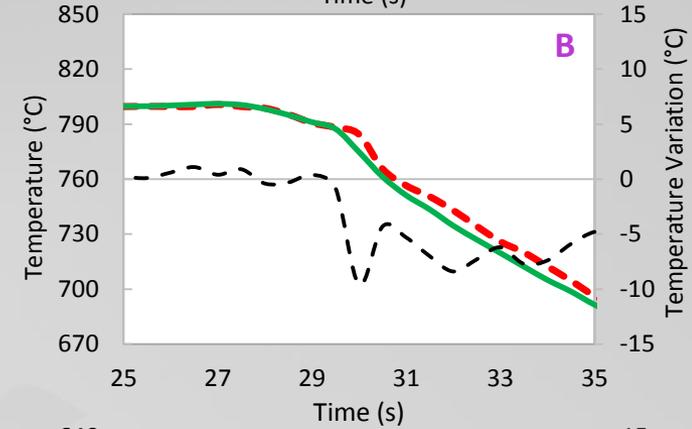
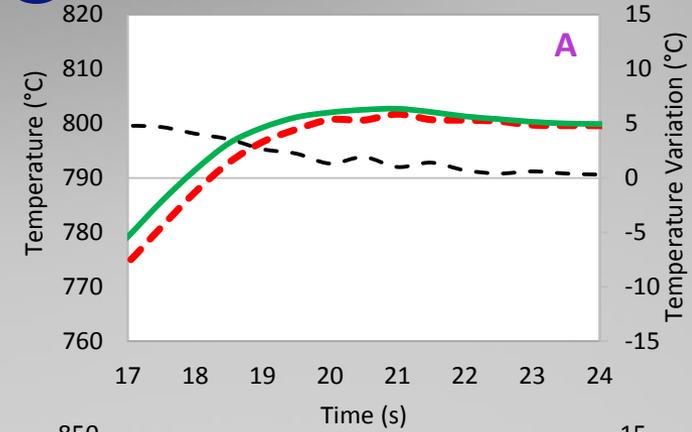
Dynamic Accuracy, IR vs TC



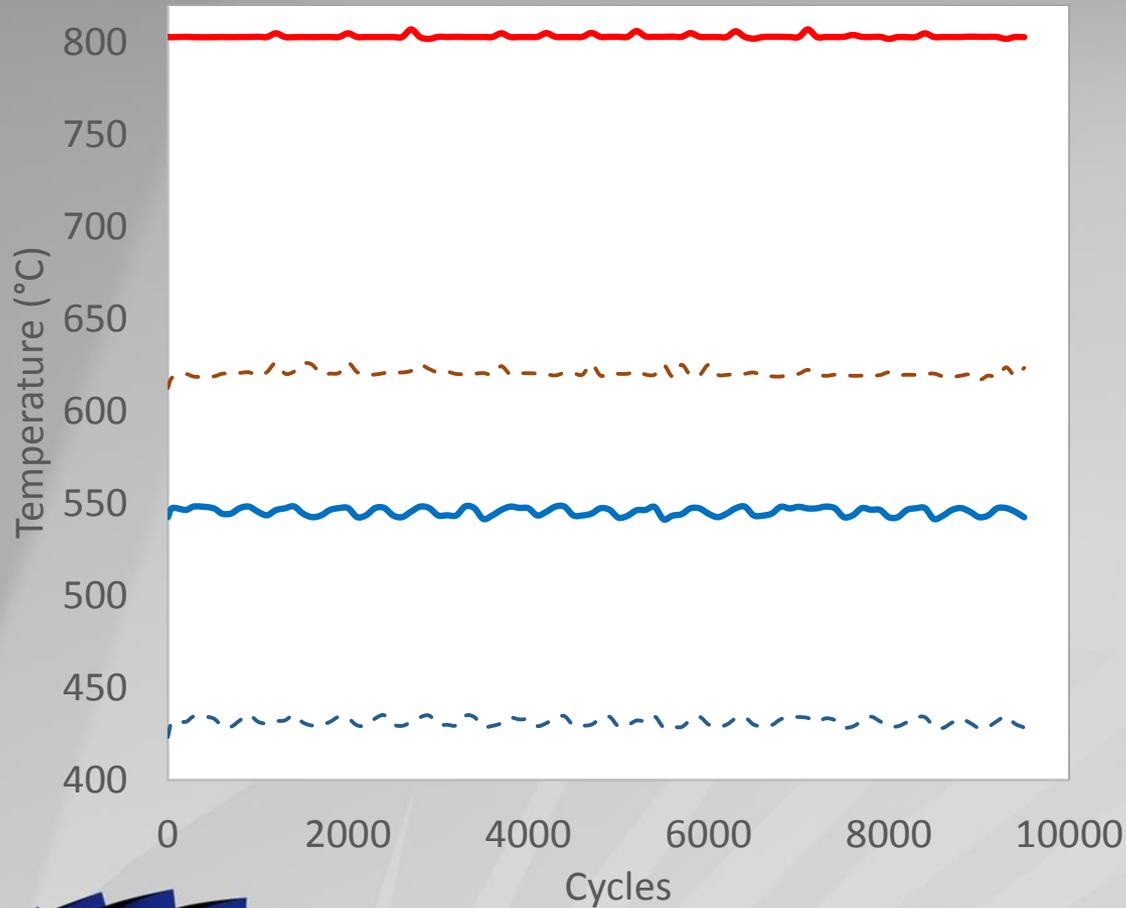
Dynamic Accuracy, IR vs TC



- IR Area Control
- TC_Center
- Temperature Deviation (°C)

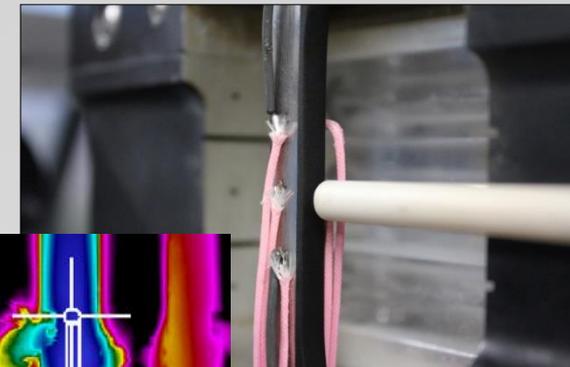


Dynamic Temperature Stability, Max/Min Cycle Peaks



- Max_IR Control
- Min_IR Control
- - - Max_TC Non Contact
- - - Min_TC Non Contact

10,000 cycles = 270 hours



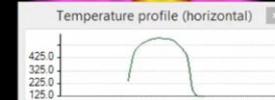
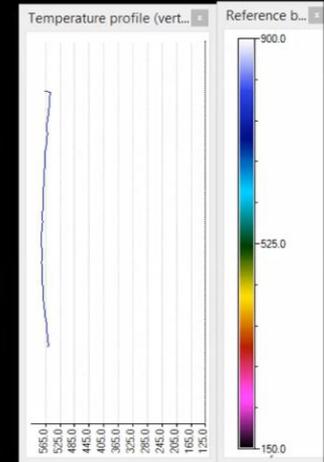
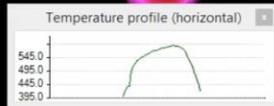
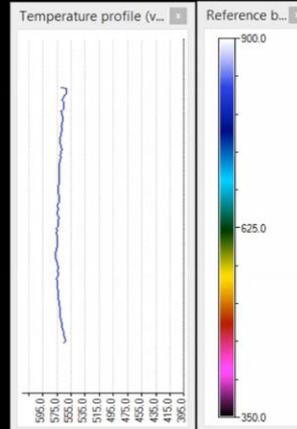
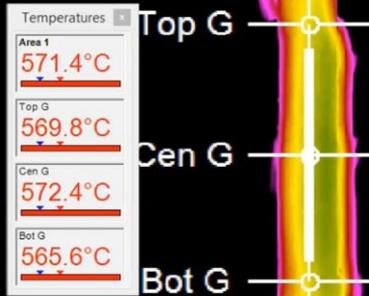
Thermocouple Complications

Thermocouples

No Thermocouples

Ø 571.4°C

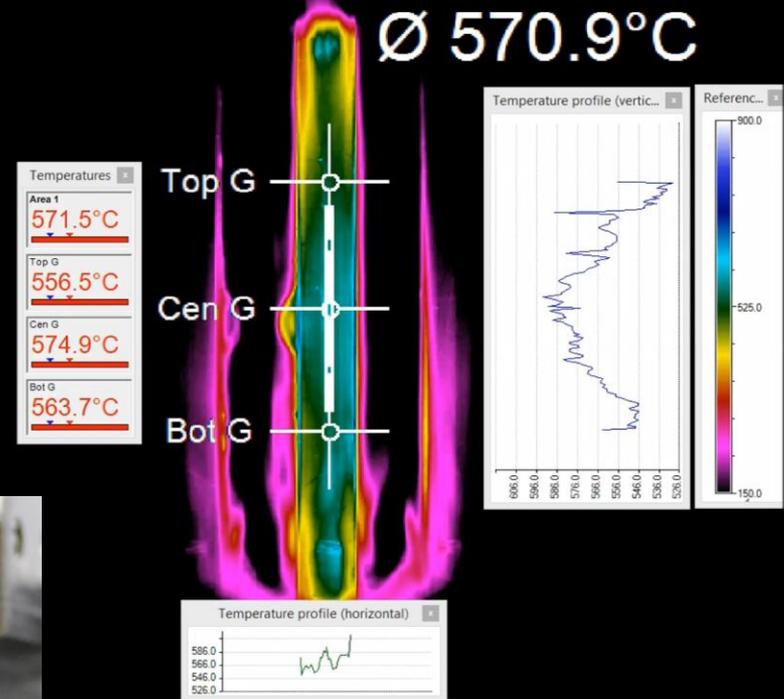
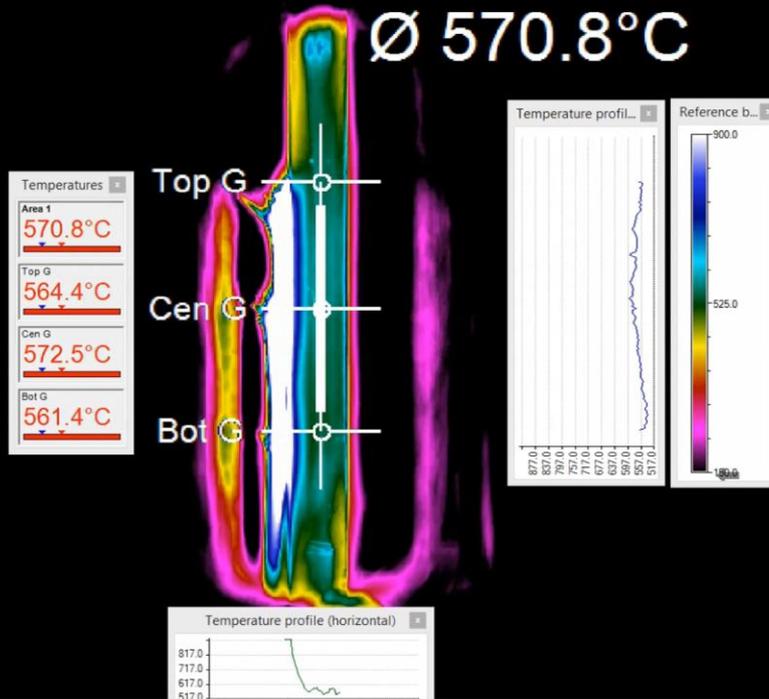
Ø 570.1°C



Evolving Surface Complications

Thermocouples

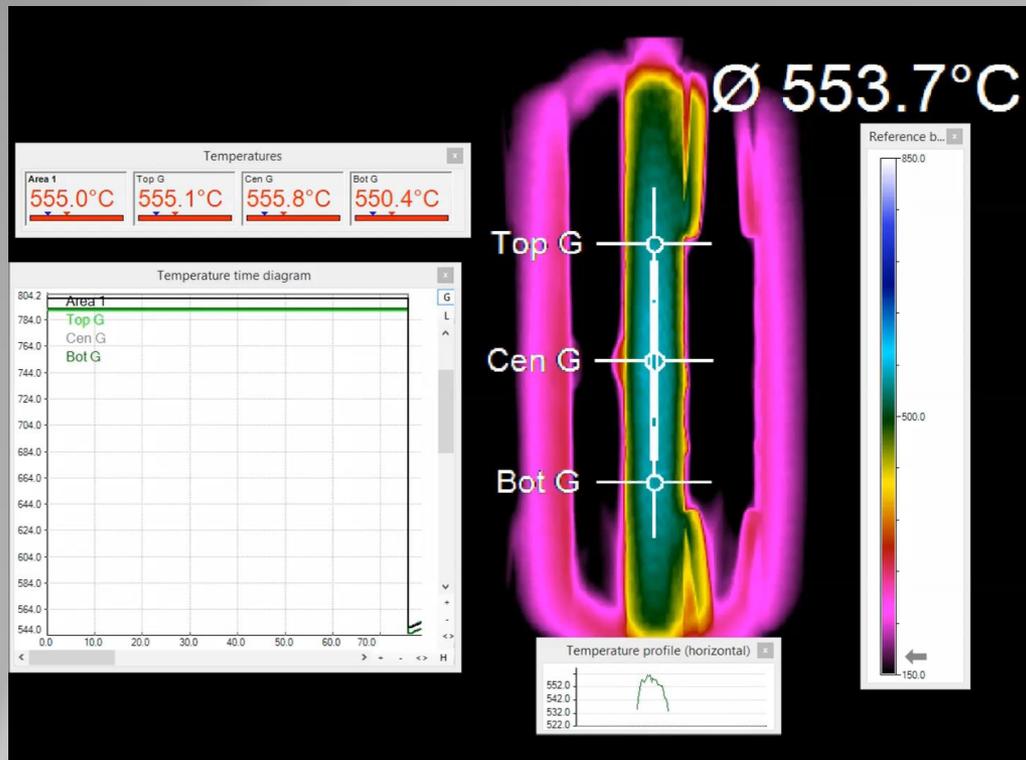
No Thermocouples



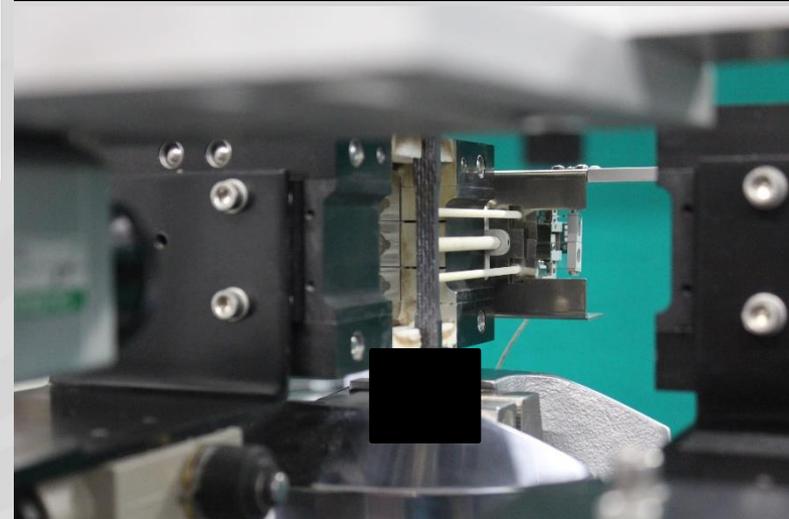
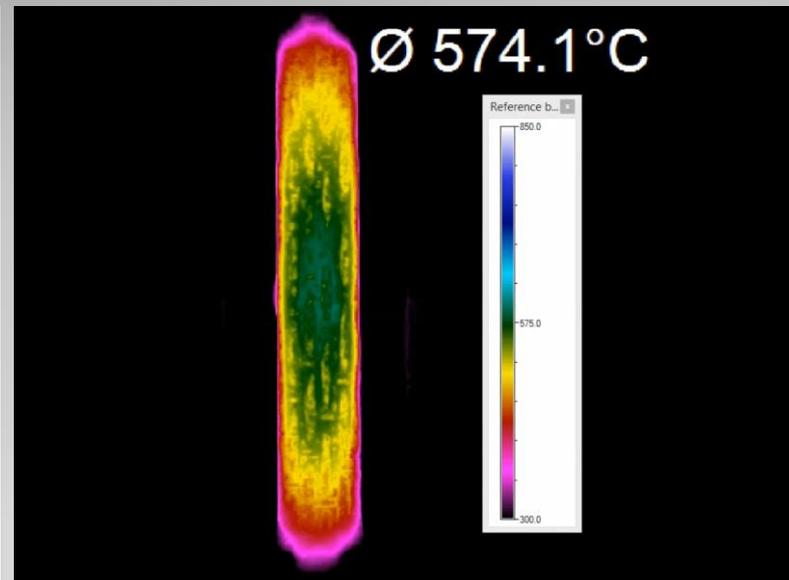
Pre-Exposed Surface
800°C for 50 hours.
 ϵ used = 0.57

Non Metallic High-Temperature Control

Specimen Side View

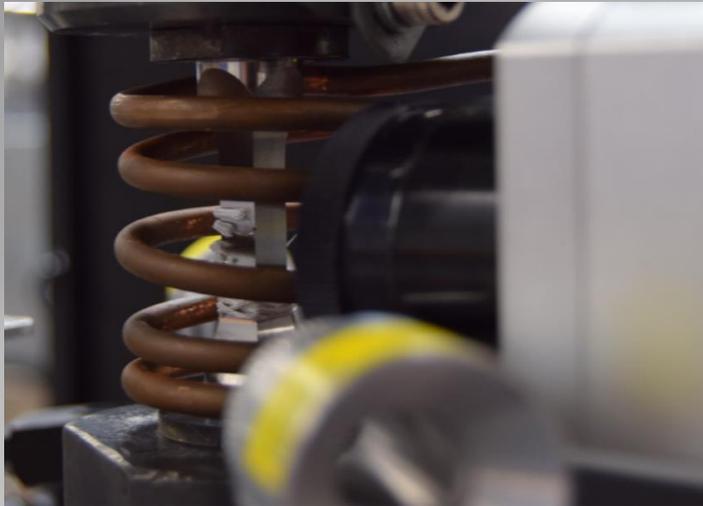


Specimen Face View

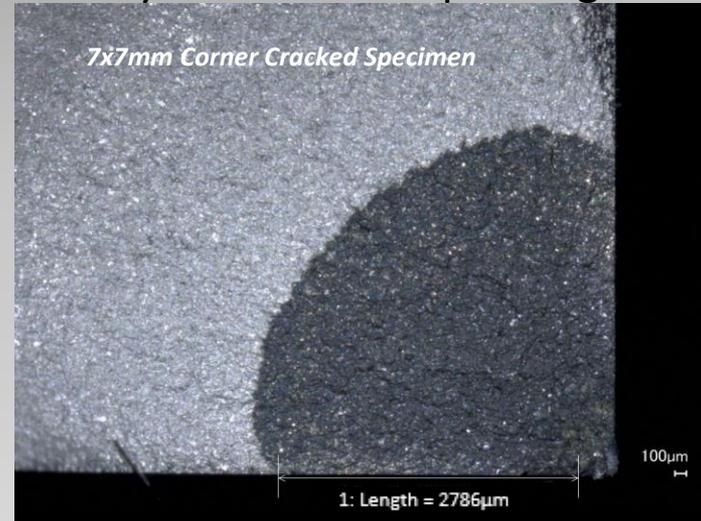


Crack Length Measurements

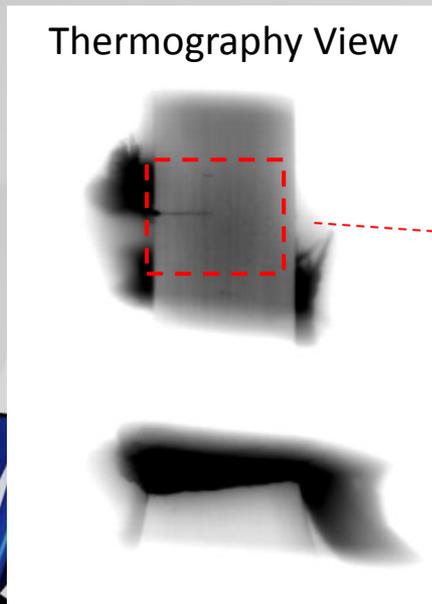
TMF Crack Growth Setup



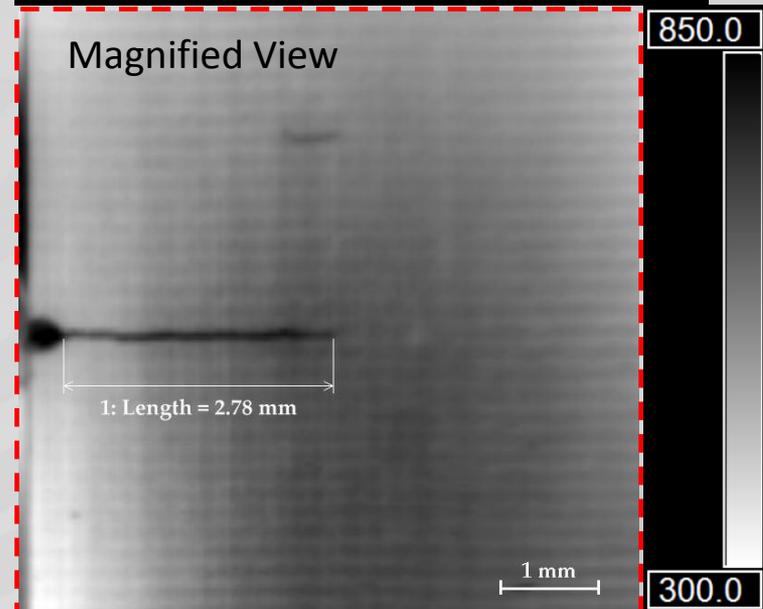
Keyence Microscope Image



Thermography View

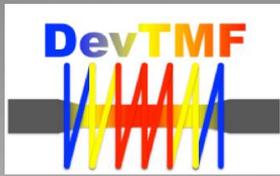


Magnified View



Conclusions: Advantages / Disadvantages

Measurement	Thermocouple	Pyrometer	Thermography
<i>Mode</i>	Invasive	Non Invasive	Non Invasive
<i>Area</i>	≈ 2mm ²	≈ 2mm ²	Entire Gauge Section
<i>Dynamic Accuracy</i>	Externally Influenced	Good	Good
<i>Set up Time</i>	Slow	Fast	Fast
<i>Profiling</i>	Thermocouple Based	Thermocouple Based	Thermography Based
<i>Repeatability</i>	Externally Influenced	Good	Good
<i>Emissivity Influenced</i>	No	Yes	Yes
<i>Post Test Analysis</i>	No	No	Yes
<i>Shadowing Effects</i>	Yes	No	No
<i>Cold Spot Identification</i>	No	No	Yes
<i>In-Situ Adjustments</i>	No	No	Yes
<i>Initial Cost</i>	Low	Ok	High
<i>Calibration Cost</i>	High	Low	Low



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Any Questions?



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