

TESTING METHODOLOGIES FOR THERMO-MECHANICAL FATIGUE EVALUATION IN ADVANCED AEROSPACE ALLOYS

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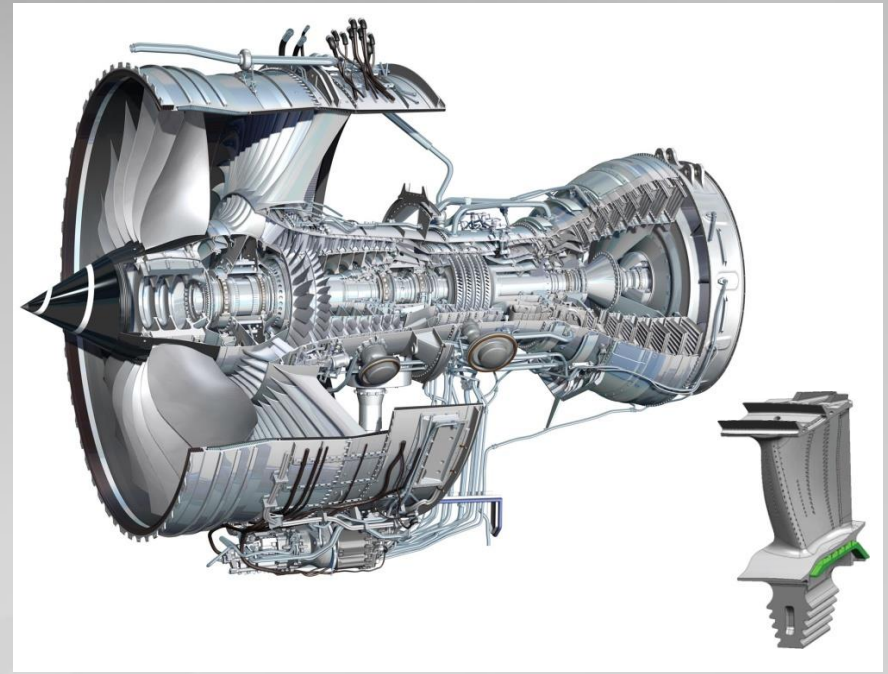
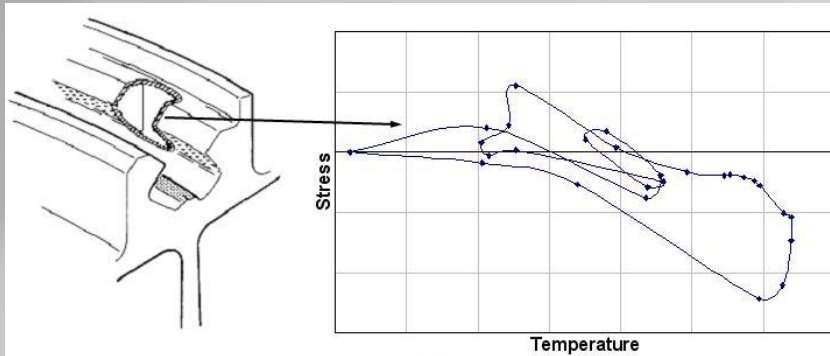
Prifysgol Abertawe
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Industrial Motivation

- Increased turbine entry temperatures
- Thinner disc rims and advanced cooling systems leading to larger thermal gradients
- Complex loading regimes within the gas turbine leading to diverse phasing between temperature and strain



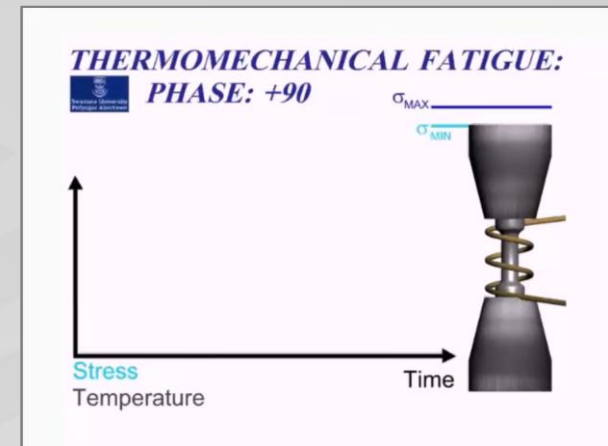
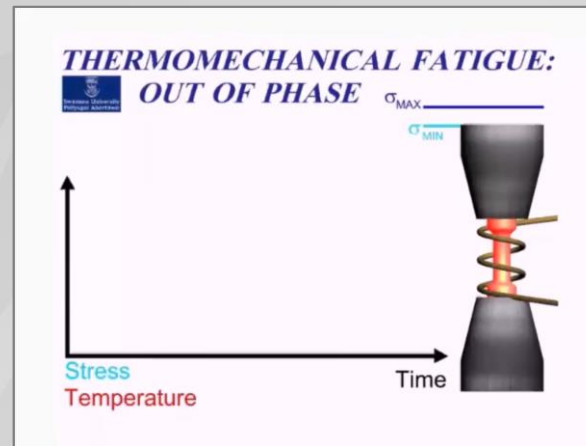
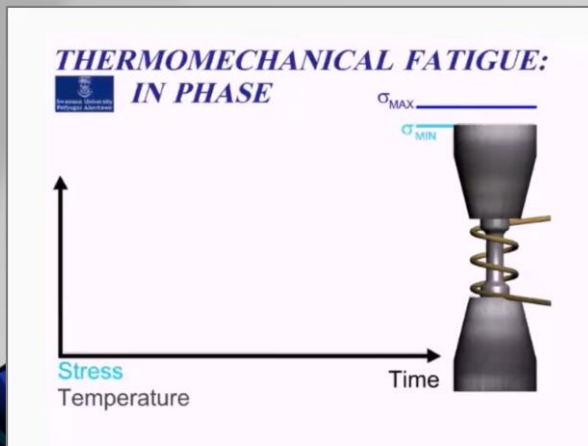
- Extrapolation of isothermal fatigue (IF) results to incorporate these effects show limited success
- Generation of TMF data is required to allow the development of lifing methodologies under TMF loading

Thermo-Mechanical Fatigue (TMF)

- Diverse mechanisms are involved, Primarily . . .

Fatigue Creep Oxidation

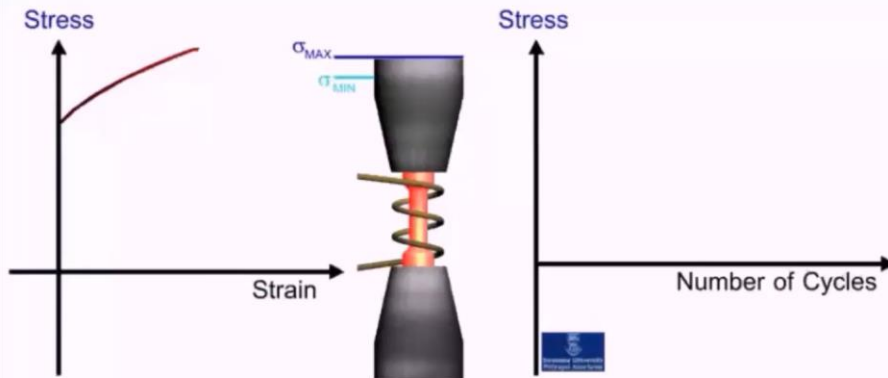
- TMF loading can be more damaging than isothermal fatigue at an equivalent T_{\max}
- Complex interaction within diverse *phase angles* between peak temperature and strain range
- Resulting in strain R ratios varying between 0 and $-\infty$ depending on the phase angle, ϕ .



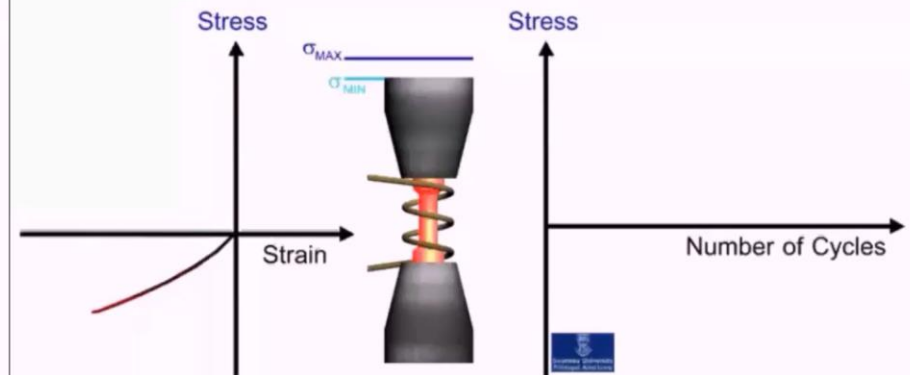
Typical TMF Hysteresis Behaviour

- Initial material behaviour may change significantly during the test.
- Understanding the stress/strain evolution throughout the test is often critical in order to be able to predict life.
- Cycle may evolve to very different stress conditions due to the interaction of plasticity and creep which often makes TMF tests differ significantly from isothermal fatigue.
- However without accurate temperature control, reliable test data for component lifing cannot be achieved.

In-Phase ($\phi = 0^\circ$)

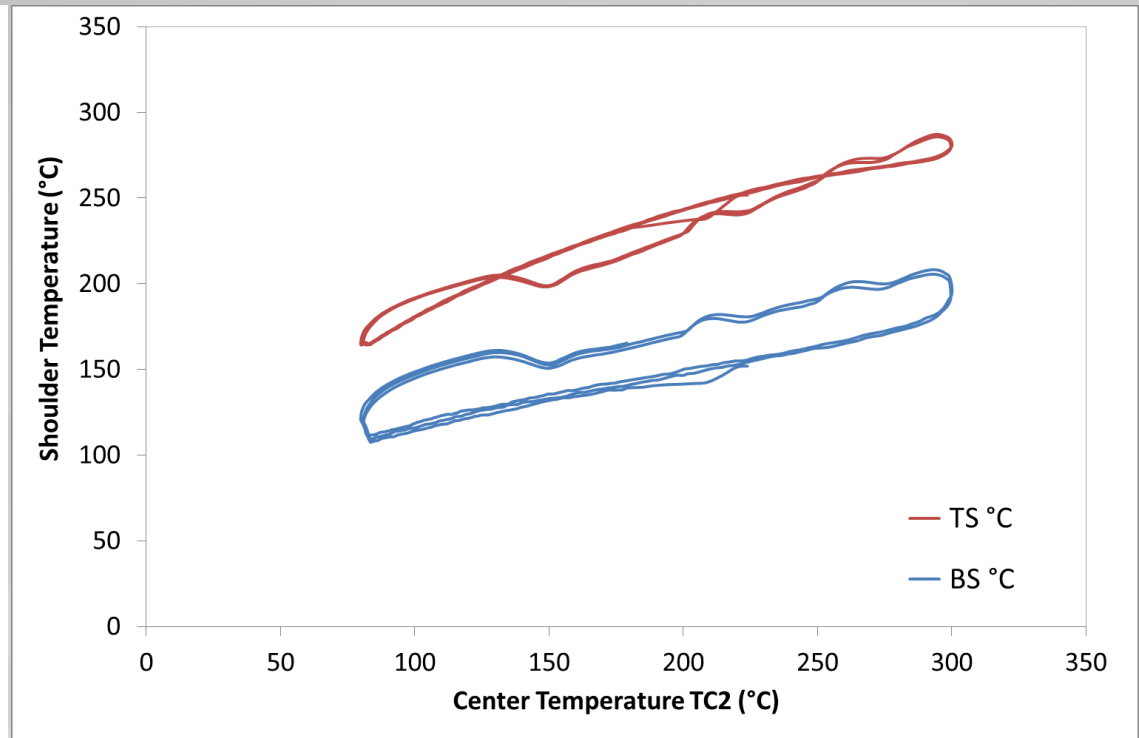
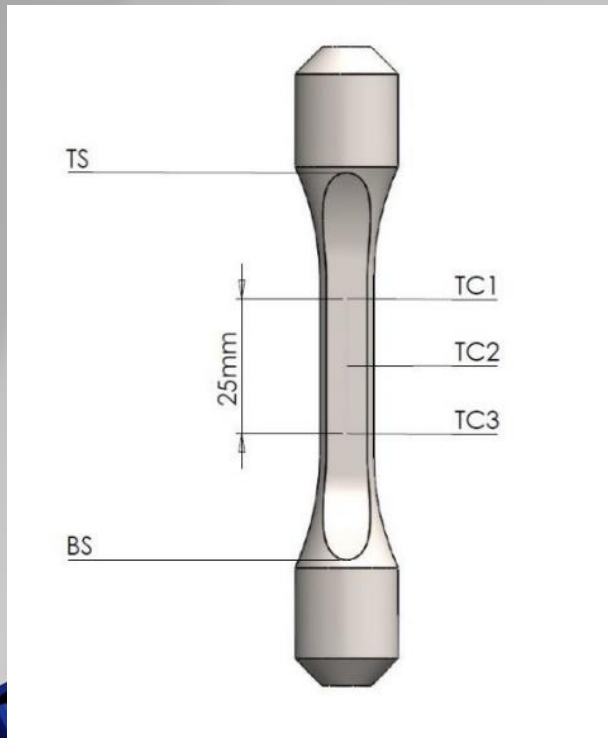


Out-Phase ($\phi = -180^\circ$)



Thermocouple Shoulder Control

- Unfavourable to weld on the specimen gauge length – Nucleation of cracks
- Contact temperature measurement can be achieved at the specimen shoulder.
- Complex setup and often temperatures at either shoulder are not stable with loops overlapping and drifting, unacceptable for temperature control purposes.



TMF Standards:

- **ASTM E2368-10:** Standard Practice for Strain Controlled Thermo-mechanical Fatigue Testing (*Released in 2004, updated in 2010*)
- **ISO 12111:2011:** Metallic materials – Fatigue Testing – Strain Controlled Thermo-mechanical Fatigue Testing Method (*Released 2011*)

Pyrometer Control

- Non-invasive temperature control can be achieved using pyrometry
- High temperature pre-exposure to produce a constant surface emissivity, ϵ .



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Pyrometer Control

- High temperature pre-exposure can reduce Fatigue life
Encinas-Oropesa, A., Drew, G. L., Hardy, M. C., Leggett, A. J., Nicholls, J. R., and Simms N. J., Proceedings of the Eleventh TMS International Symposium, Superalloys, pp. 609-618, 2008
- Thermal Profiling still achieved using thermocouples

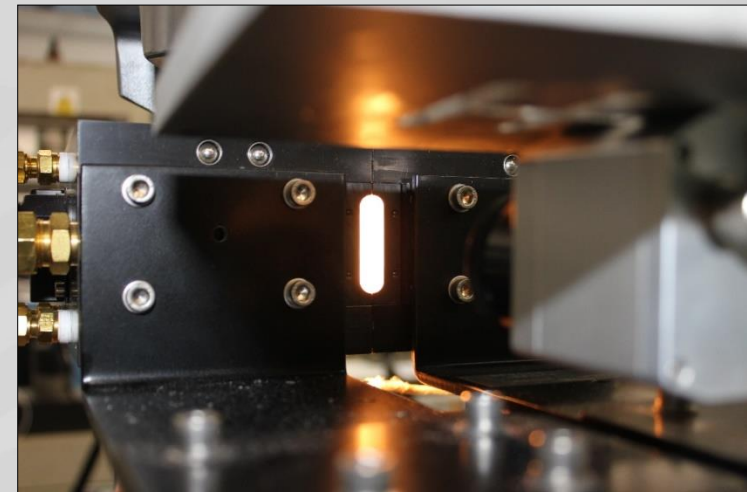
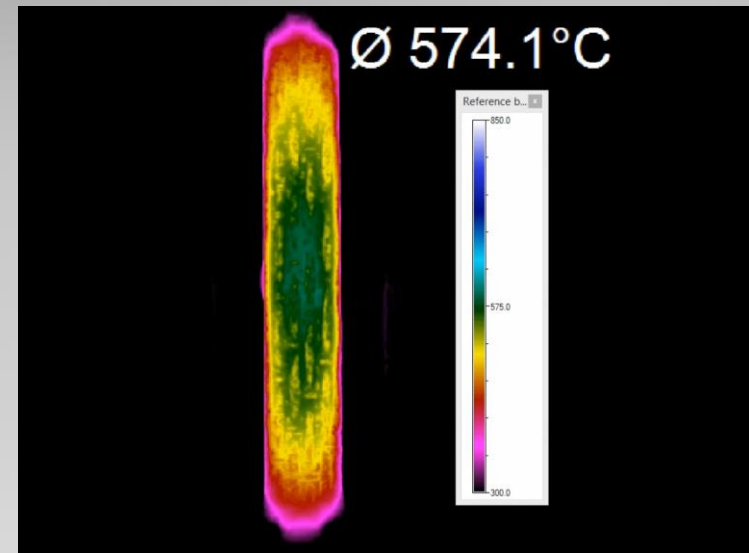


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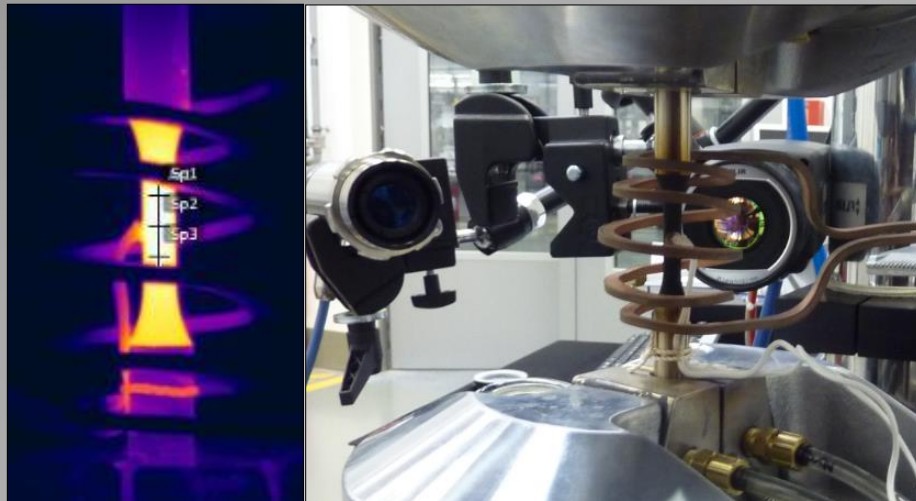
Introduction - Thermography

- Technique that can deliver....
 - Accurate Temperature control
 - Incorporates Thermal Profiling
 - Not influenced by Surface emissivity
 - Completely Non-Invasive
 - Metallic and non-metallic materials
 - Robust and repeatable
- Infra-red, Thermography?

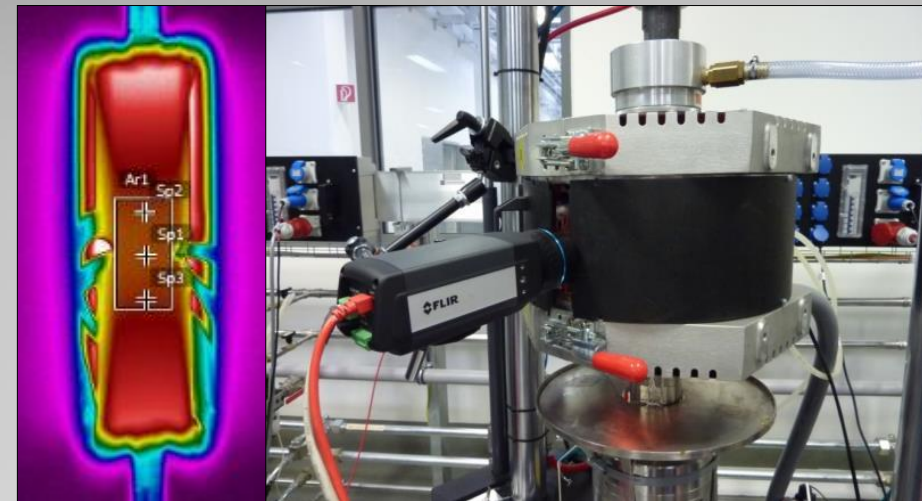


Previous Work – Rolls-Royce plc, MTOC, Germany

Induction Heating



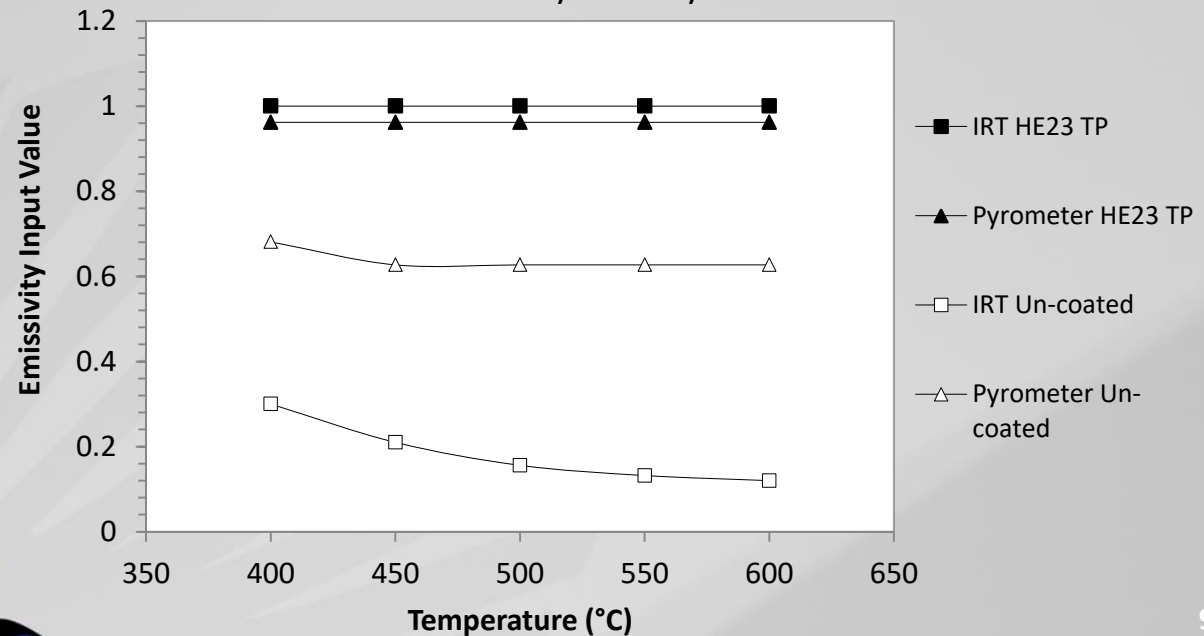
Radiant Lamp Furnace Heating



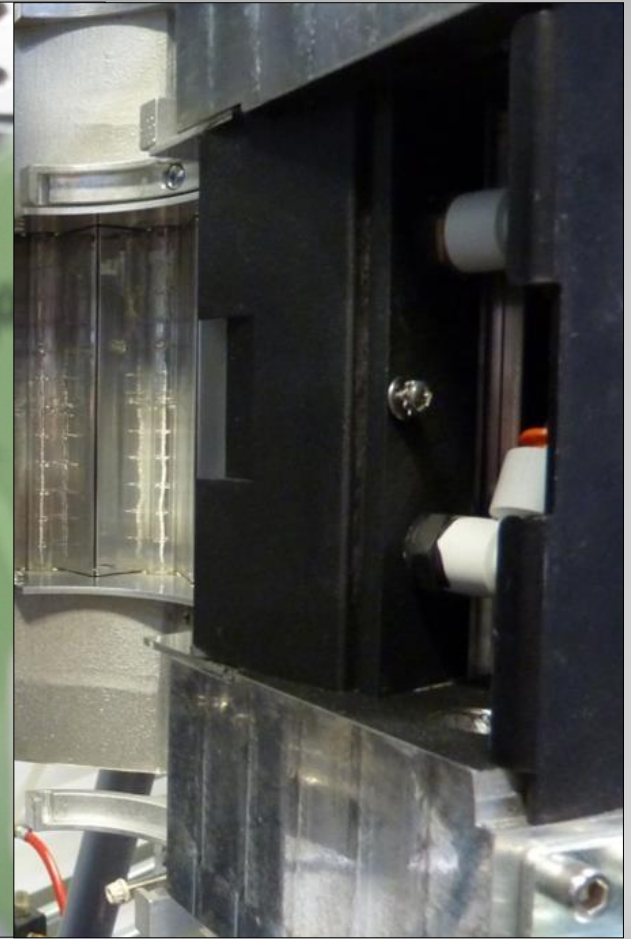
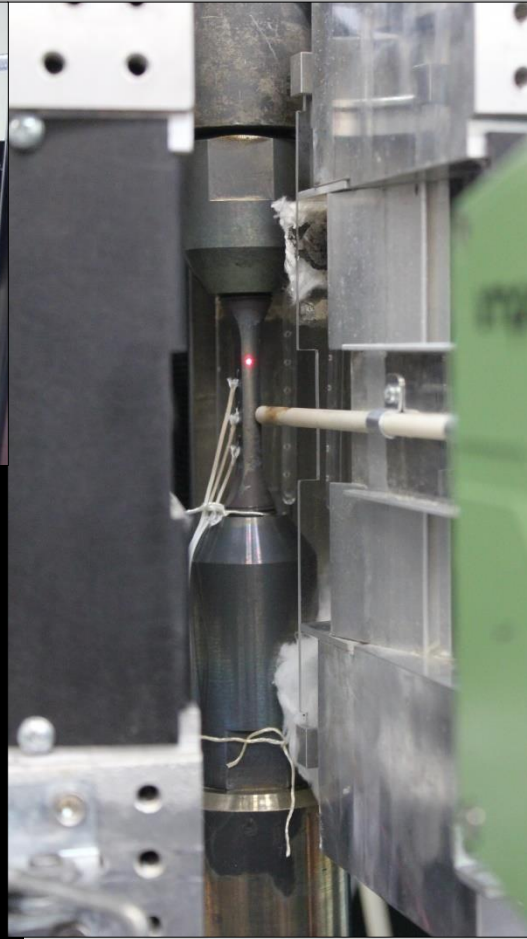
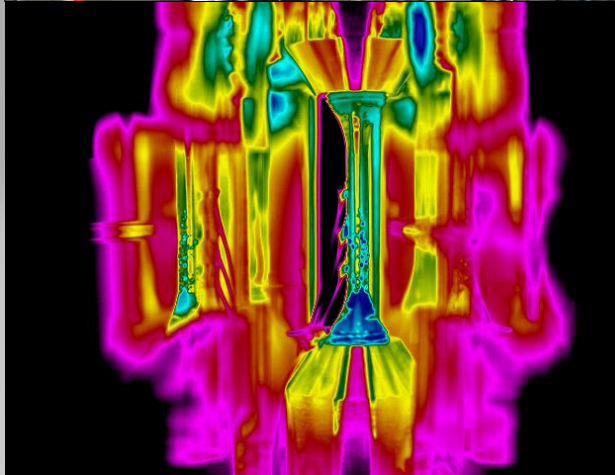
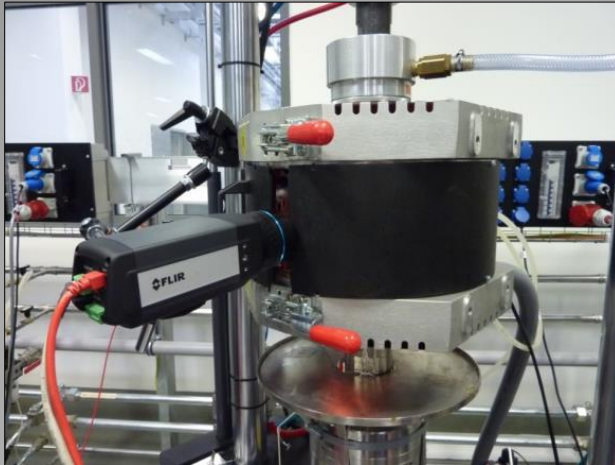
HE23 Thermal Paint



Surface Emissivity Stability



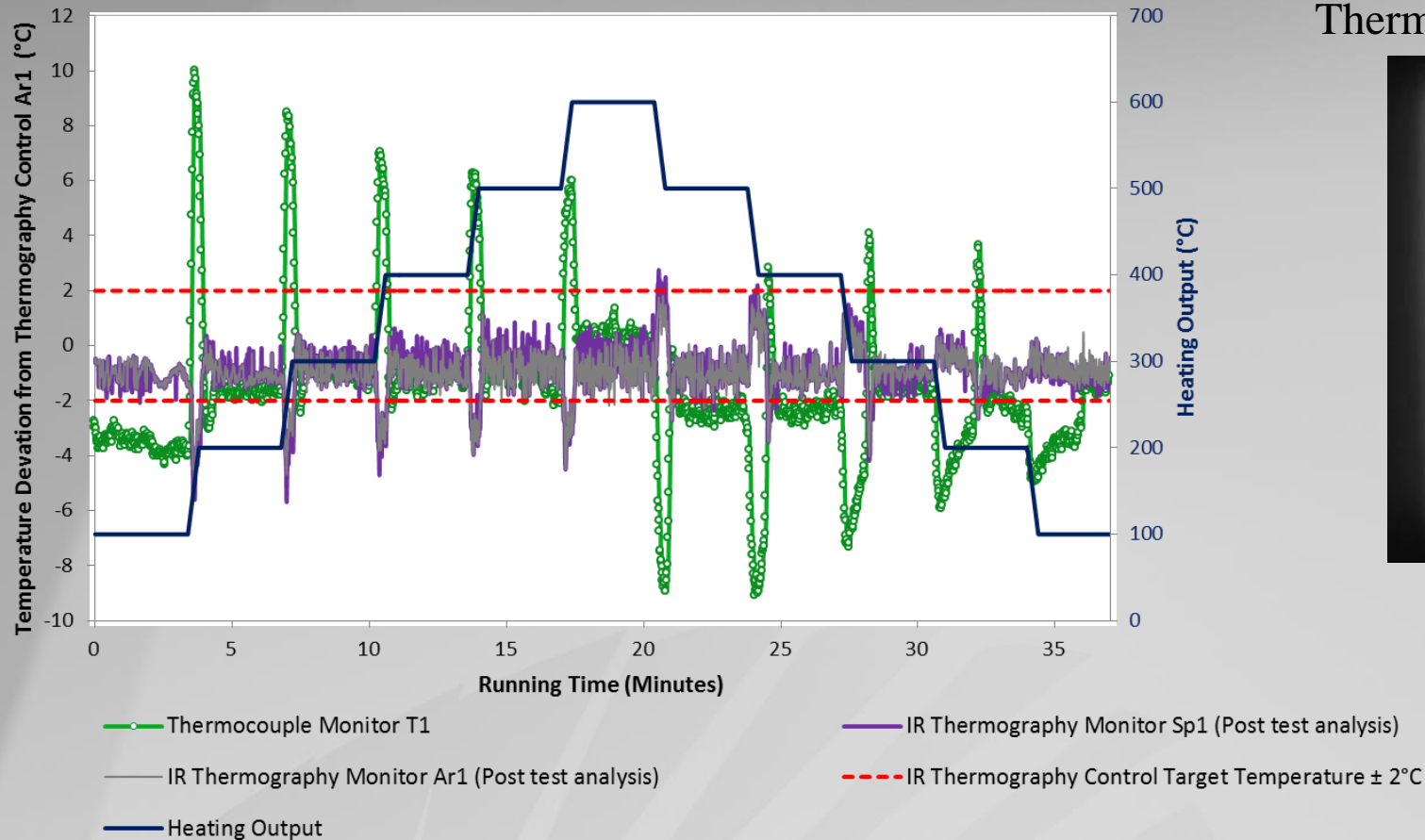
Previous Work – Radiation Reflections



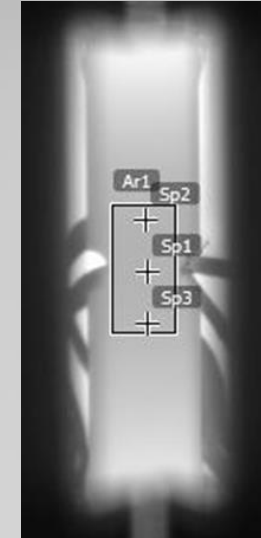
Jones, J.P., et al., Non-invasive temperature measurement and control techniques under thermomechanical fatigue loading. *Materials Science and Technology* **2014**. 30(15): p. 1862-1876

Jones, J.P., et al. Assessment of Infrared Thermography for Cyclic High-Temperature Measurement and Control. in 4th Evaluation of Existing and New Sensor Technologies for Fatigue, Fracture and Mechanical Testing. **2015**. Toronto: ASTM International.

Previous Work – Thermography vs Thermocouples

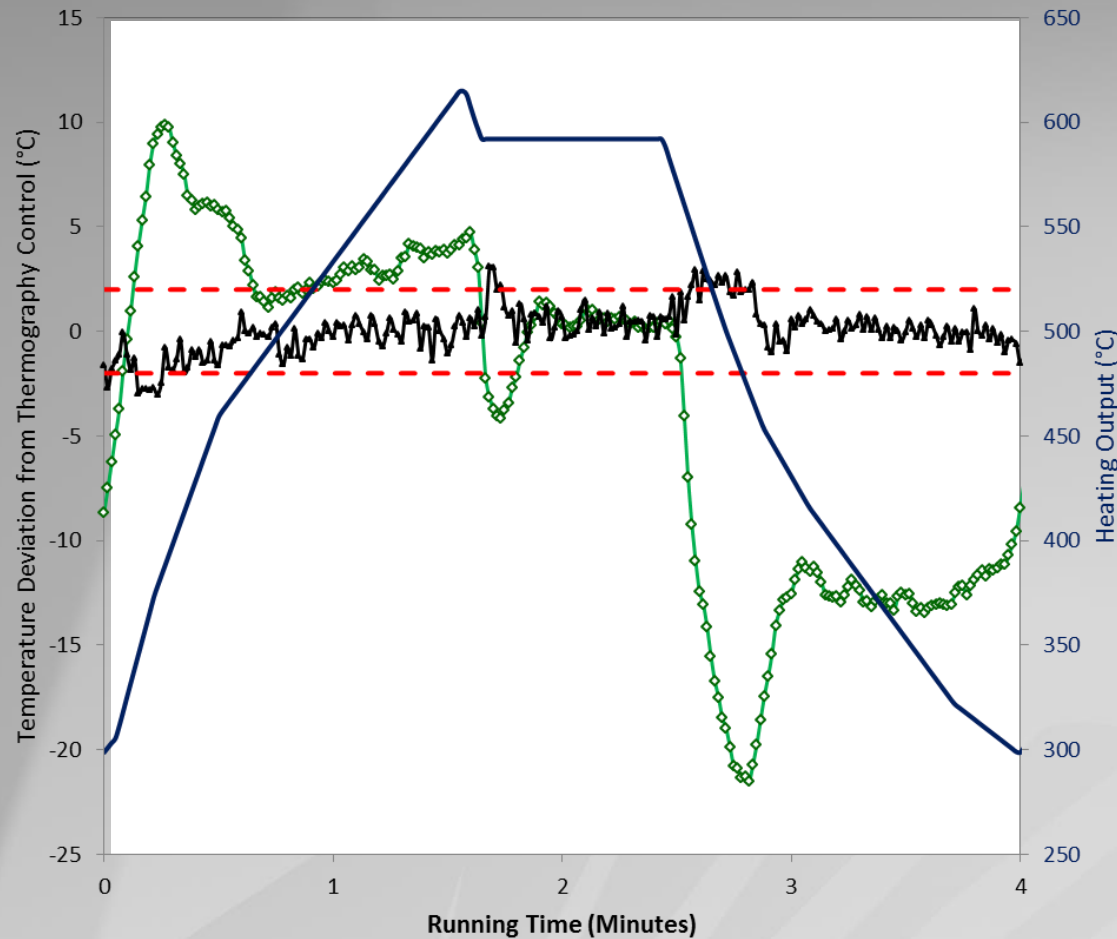


Thermography View

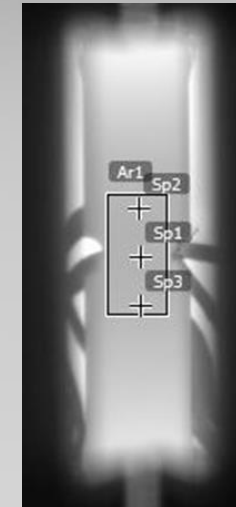


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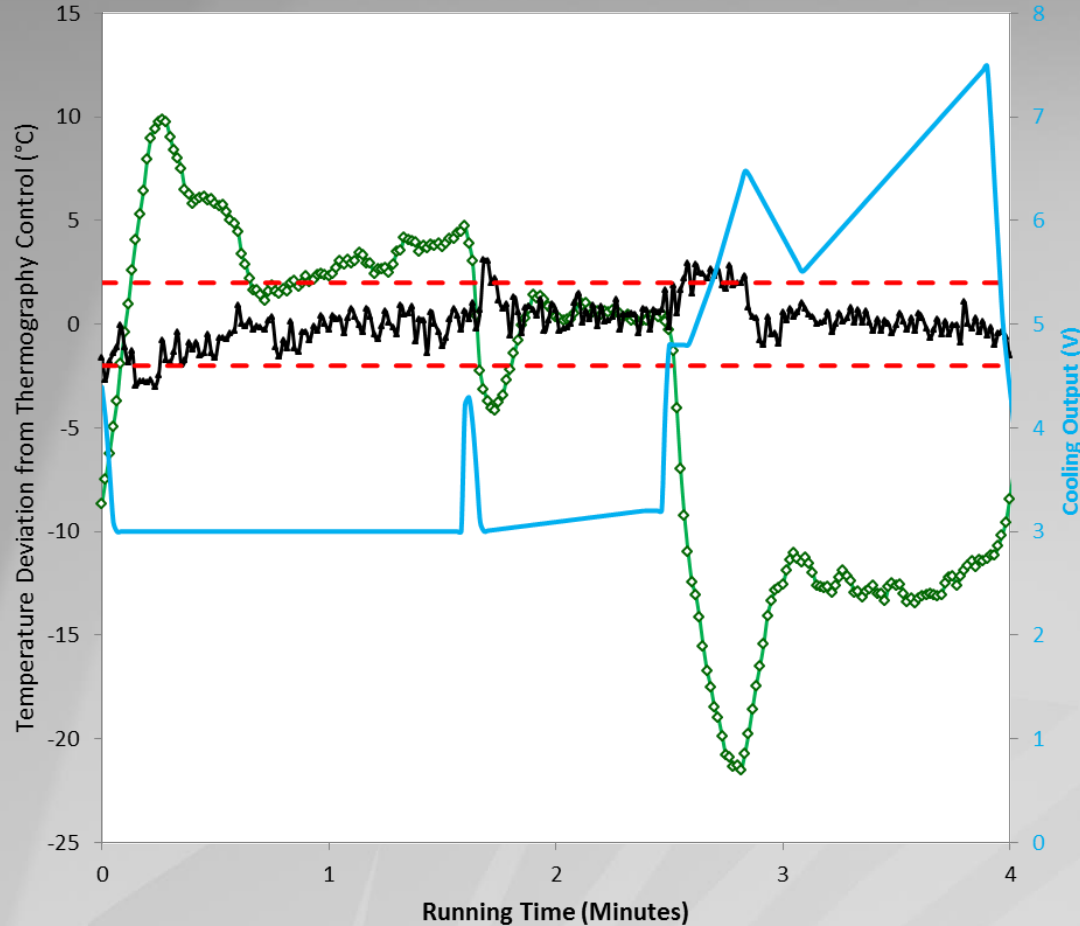
Thermography View



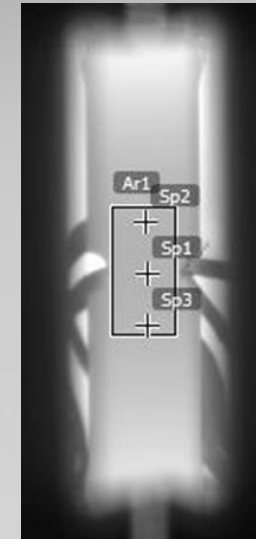
- ◆— Thermocouple Monitor TC1
- IR Thermography Monitor Sp1 (Post test analysis)
- - - IR Thermography Control Ar1 Target Temperature $\pm 2^{\circ}\text{C}$
- Heating Output

- Jones, J.P., et al., Non-invasive temperature measurement and control techniques under thermomechanical fatigue loading. *Materials Science and Technology* **2014**. 30(15): p. 1862-1876
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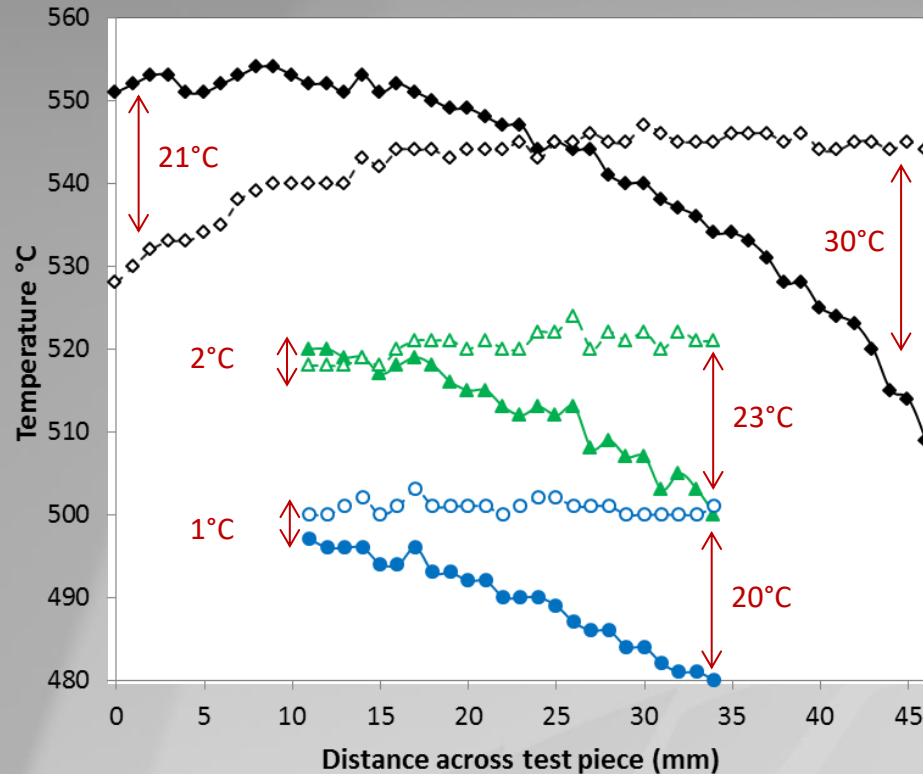
Thermography View



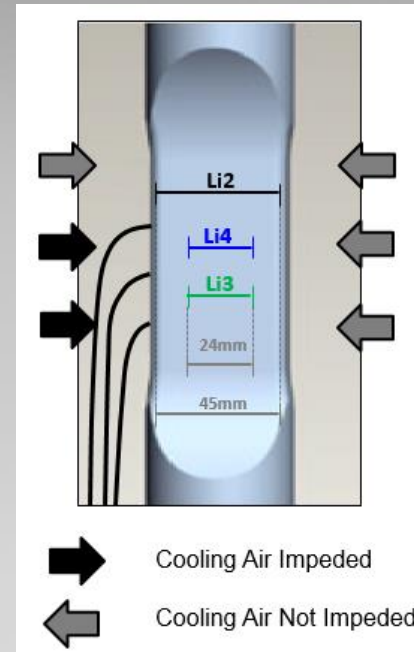
- Thermocouple Monitor TC1
- IR Thermography Monitor Sp1 (Post test analysis)
- IR Thermography Control Ar1 Target Temperature $\pm 2^{\circ}\text{C}$
- Cooling Output

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Previous Work – Thermocouple Shadowing

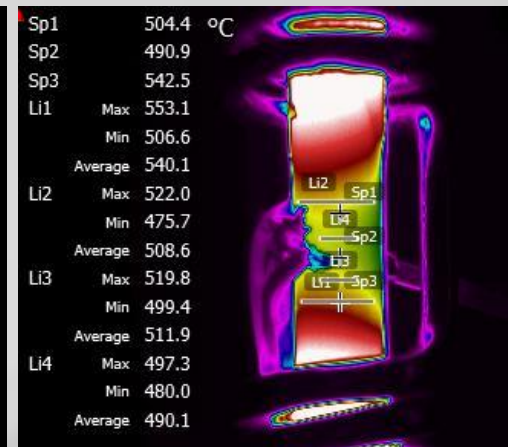
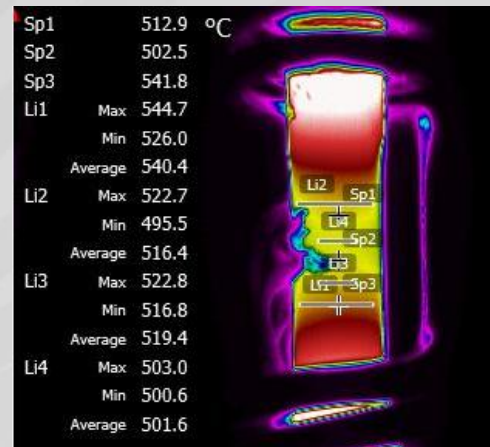


- Li1 Not Impeded
- ▲— Li3 Not Impeded
- Li4 Not Impeded
- ◇— Li1 Air Impeded
- △— Li3 Air Impeded
- Li4 Air Impeded

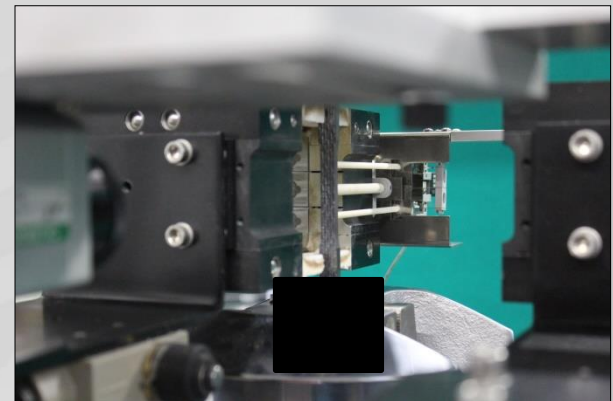
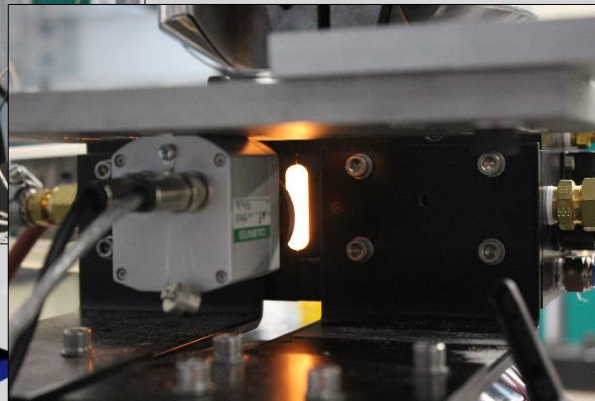
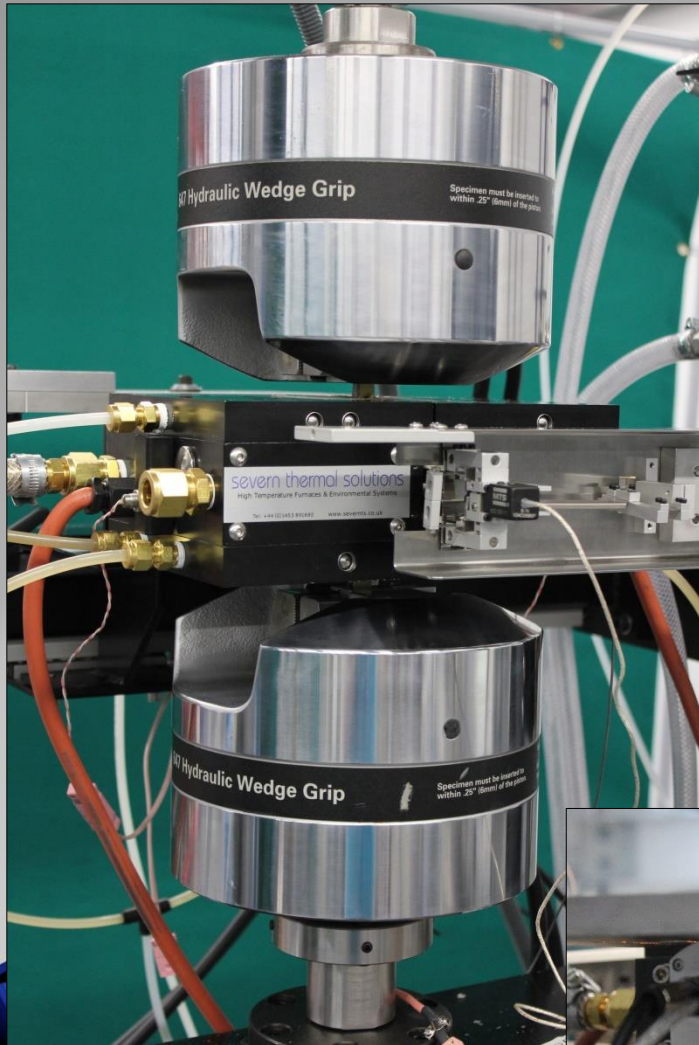


Cooling Direction

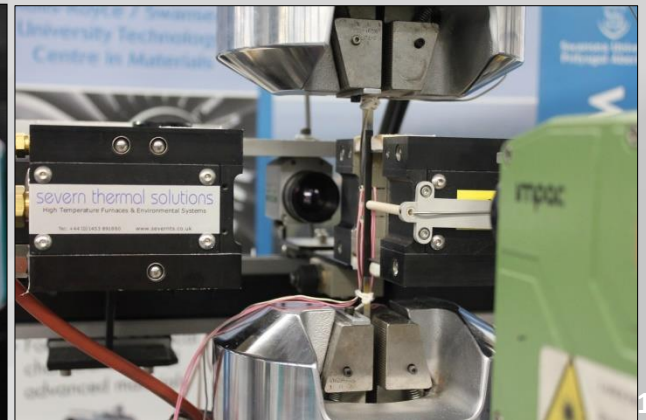
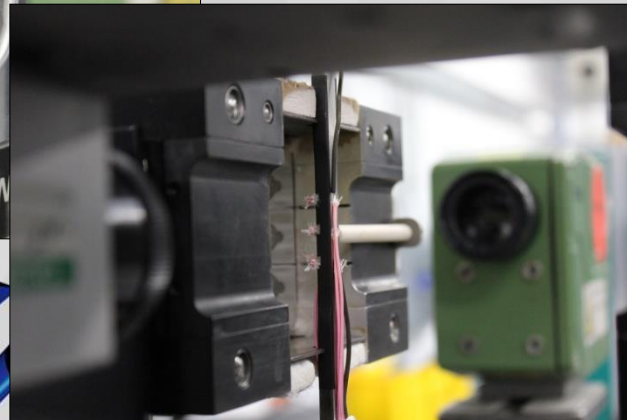
Cooling Direction



Bespoke TMF Setup – Non Metallic Materials



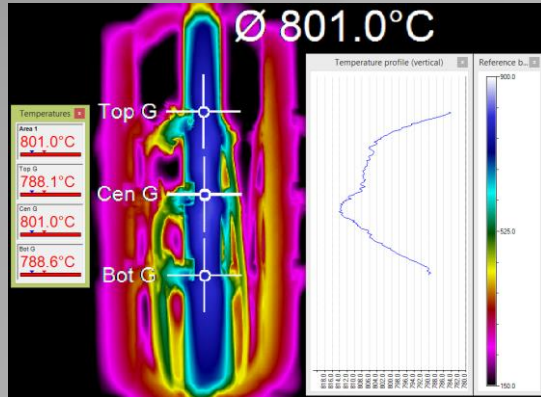
Bespoke TMF Setup – Non Metallic Materials



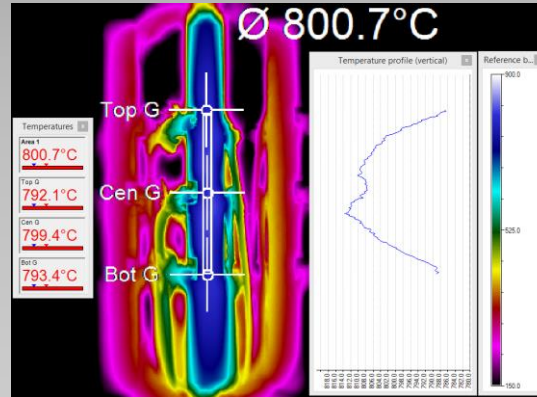
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Control Method Comparison

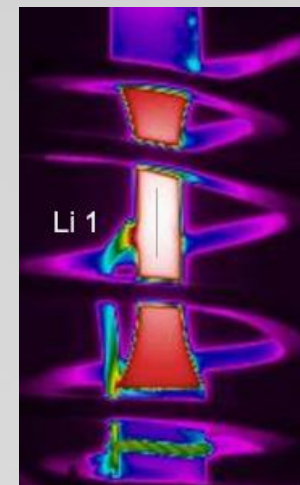
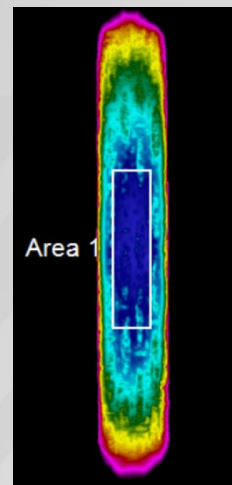
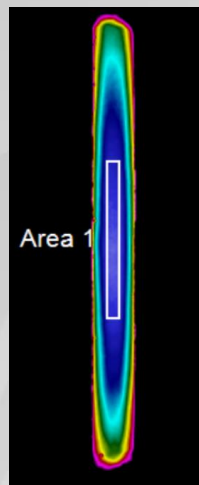
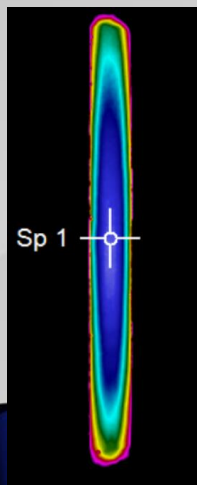
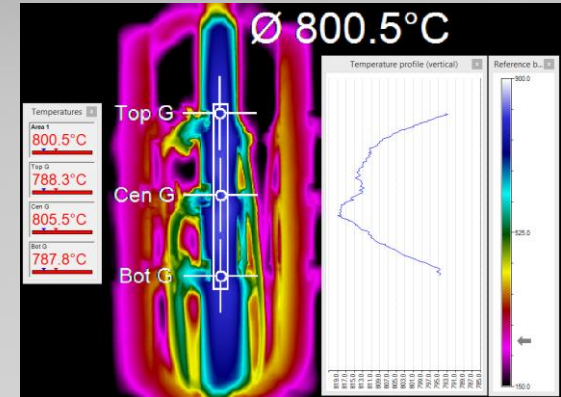
Single Point Control



Small Area Control (2 x 25mm)

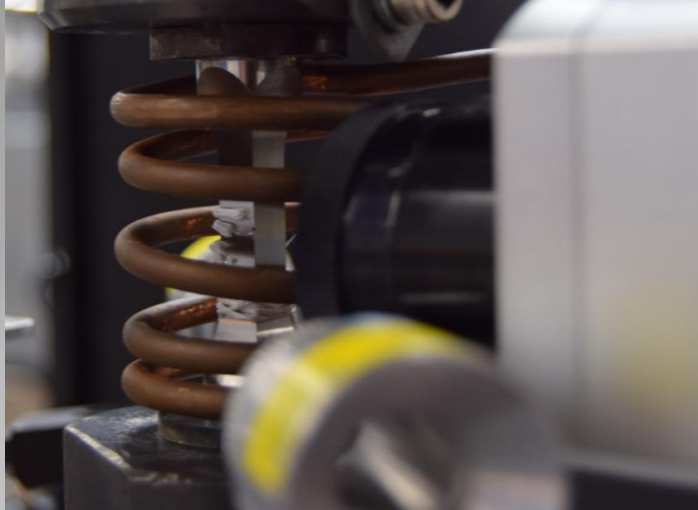


Large Area Control (3 x 30mm)

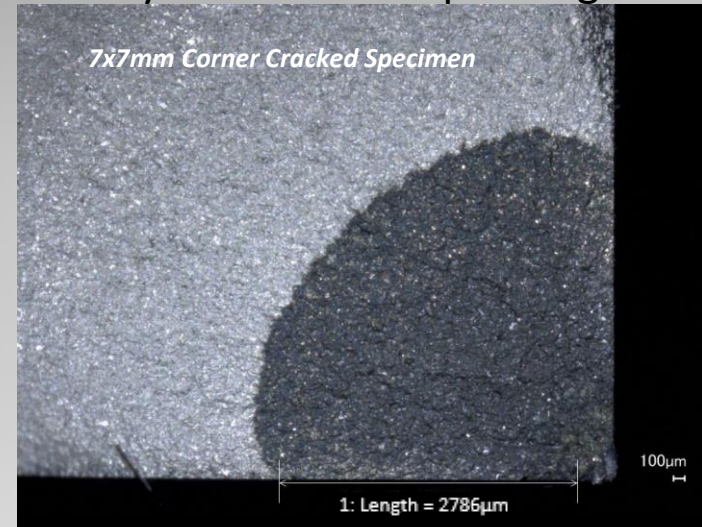


Crack Length Measurements

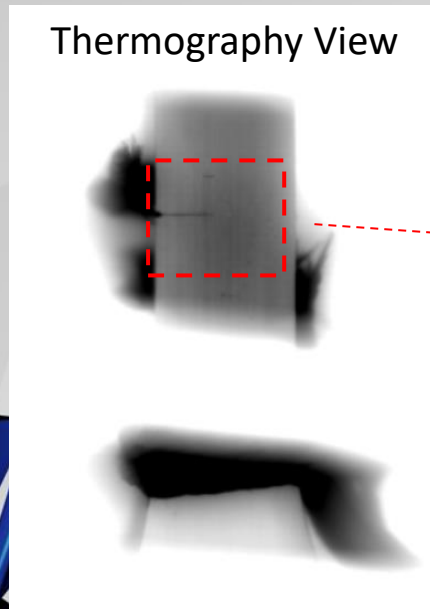
TMF Crack Growth Setup



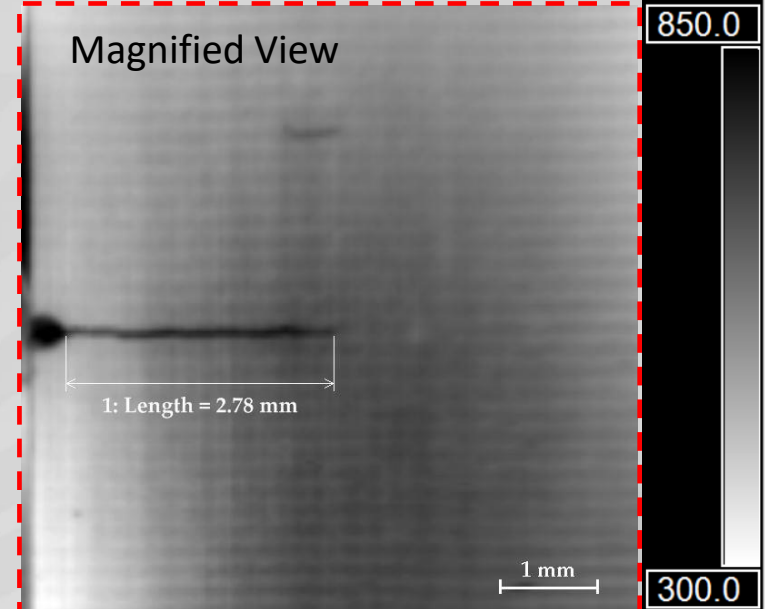
Keyence Microscope Image



Thermography View



Magnified View



Conclusions: Advantages / Disadvantages

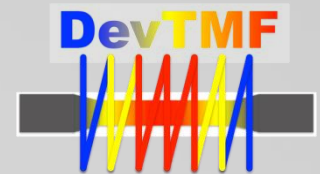
Measurement	Thermocouple	Pyrometer	Thermography
Mode	Invasive	Non Invasive	Non Invasive
Area	≈ 2mm ²	≈ 2mm ²	Entire Gauge Section
Dynamic Accuracy	Externally Influenced	Good	Good
Set up Time	Slow	Fast	Fast
Profiling	Thermocouple Based	Thermocouple Based	Thermography Based
Repeatability	Externally Influenced	Good	Good
Emissivity Influenced	No	Yes	Yes
Post Test Analysis	No	No	Yes
Shadowing Effects	Yes	No	No
Cold Spot Identification	No	No	Yes
In-Situ Adjustments	No	No	Yes
Initial Cost	Low	Ok	High
Calibration Cost	High	Low	Low

Acknowledgements

This project has received funding from the European Union's Horizon 2020 research and innovation programme and Joint Undertaking Clean Sky 2 under grant agreement No 686600. The provision of materials and technical support from Rolls-Royce plc is gratefully acknowledged. A special mention must be paid to Veronica Gray, Turan Dirlik and Nigel Ryder.

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Any Questions?



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