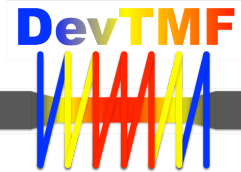


# Thermomechanical fatigue crack initiation in disc alloys using a damage approach

Daniel Leidermark<sup>1</sup>, Robert Eriksson<sup>1</sup>, James Rouse<sup>2</sup>,  
Christopher Hyde<sup>2</sup>, Sjetlana Stekovic<sup>1</sup>

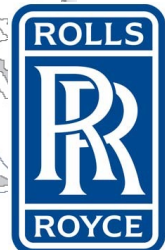
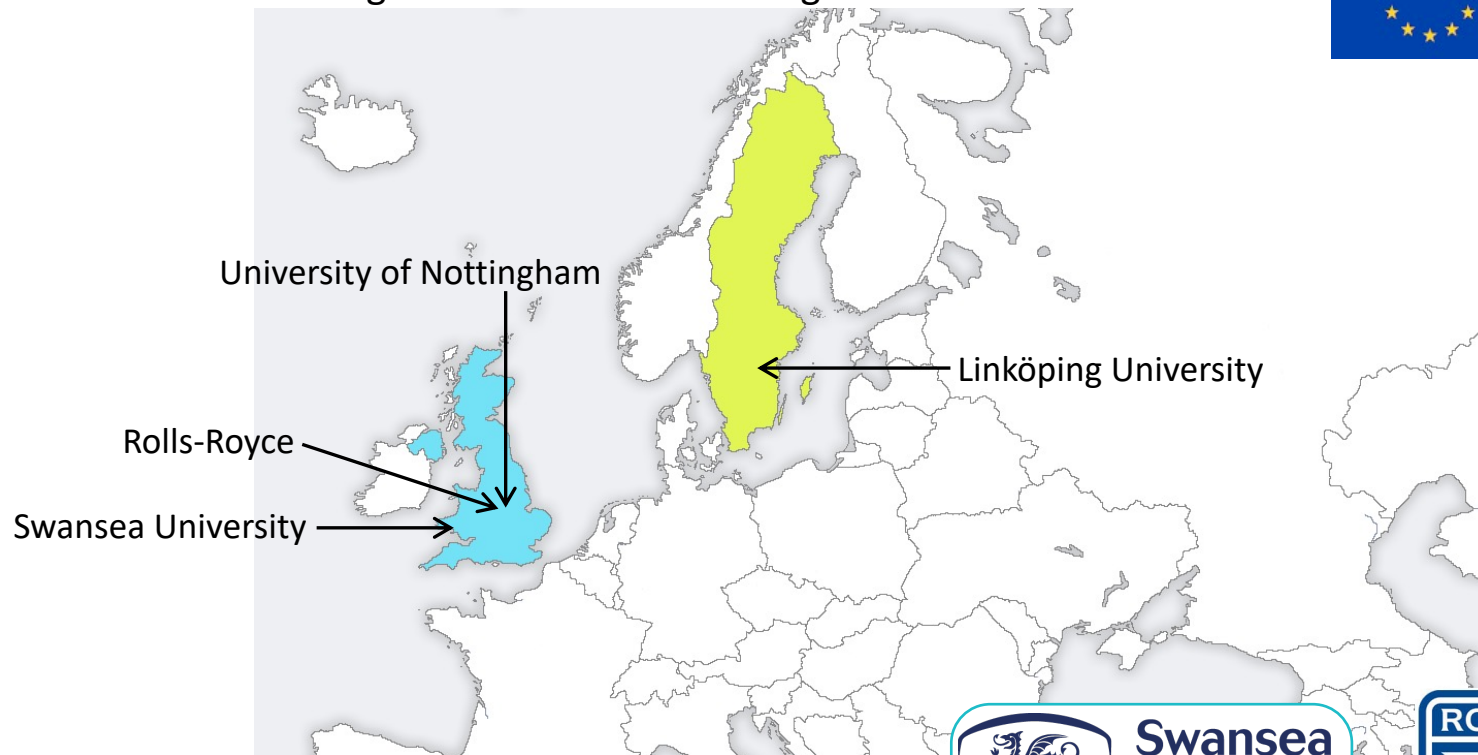
<sup>1</sup>Division of Solid Mechanics, Linköping University

<sup>2</sup>G2TRC, University of Nottingham

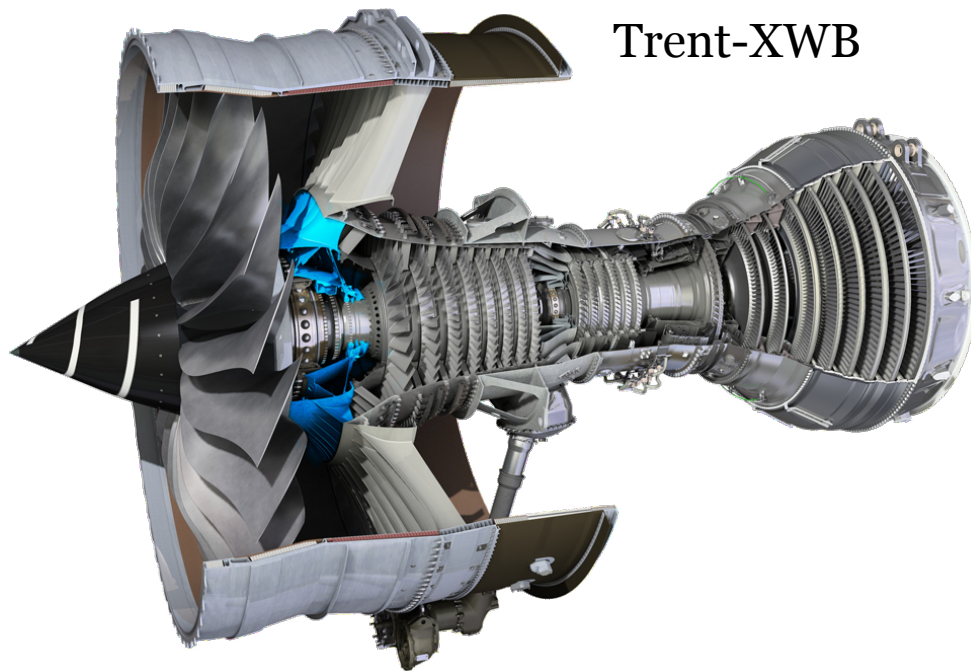


# DevTMF – Horizon 2020 – CleanSky 2

**Dev**elopment of Experimental Techniques and Predictive Tools to Characterise Thermo**M**echanical **F**atigue Behaviour and Damage Mechanisms



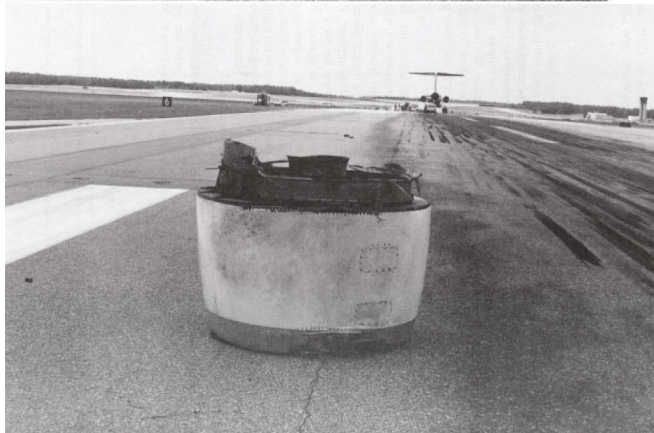
# Gas turbine



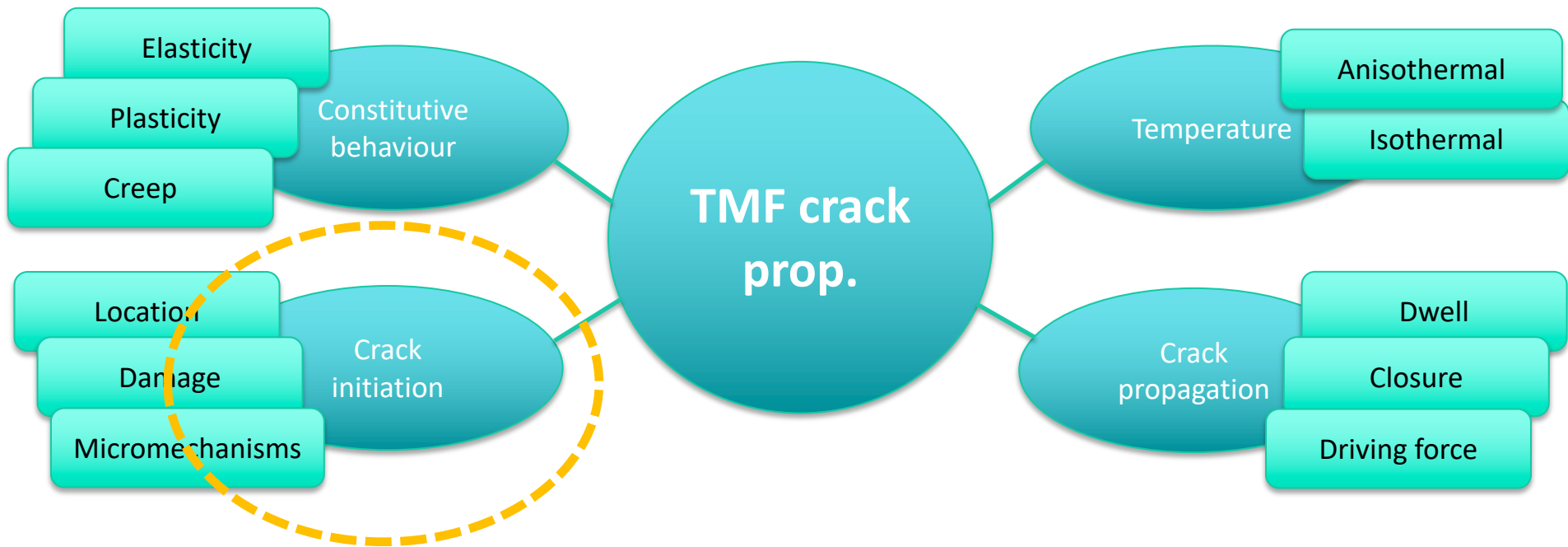
Trent-XWB

SGT-800

# Failure is not an option



# DevTMF



# TMF crack initiation experiments

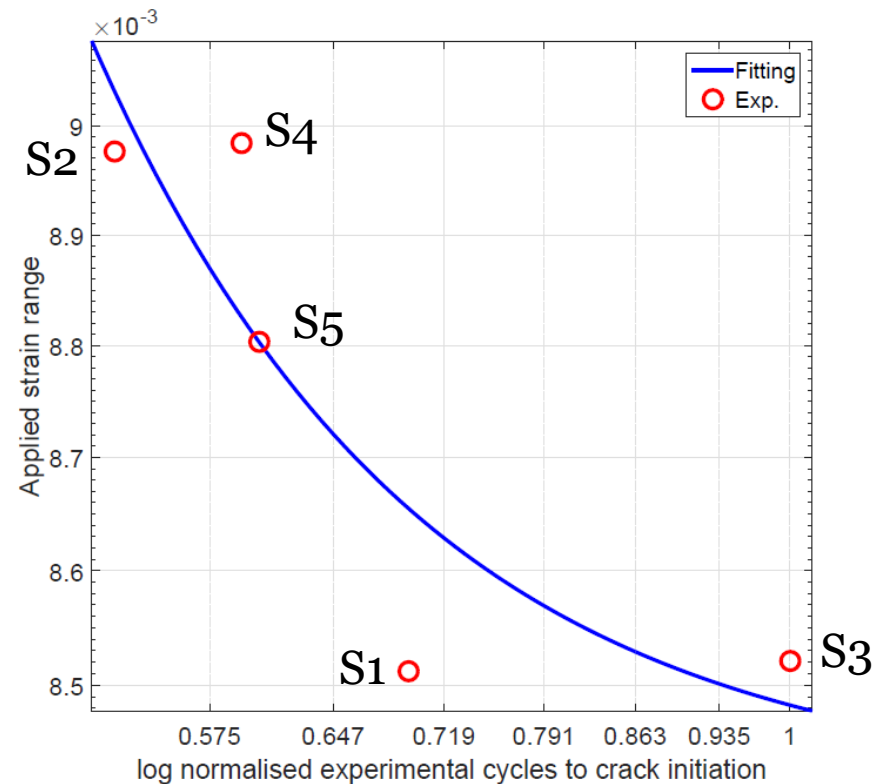
- Polycrystalline Ni-base disc alloy: RR1000
- Smooth round specimens
- Engine relevant load cycle:
  - ”OP”-TMF: 300 – 675 °C
  - Hold-time: 30s

10% load-drop

Specimen	Diameter [mm]	$\Delta\varepsilon_{mech}$ [%]	Normalised $N_i$
<i>S1</i>	7.61	0.8512	0.695
<i>S2</i>	7.60	0.8976	0.526
<i>S3</i>	7.62	0.8521	1.000
<i>S4</i>	7.60	0.8984	0.593
<i>S5</i>	7.61	0.8803	0.604

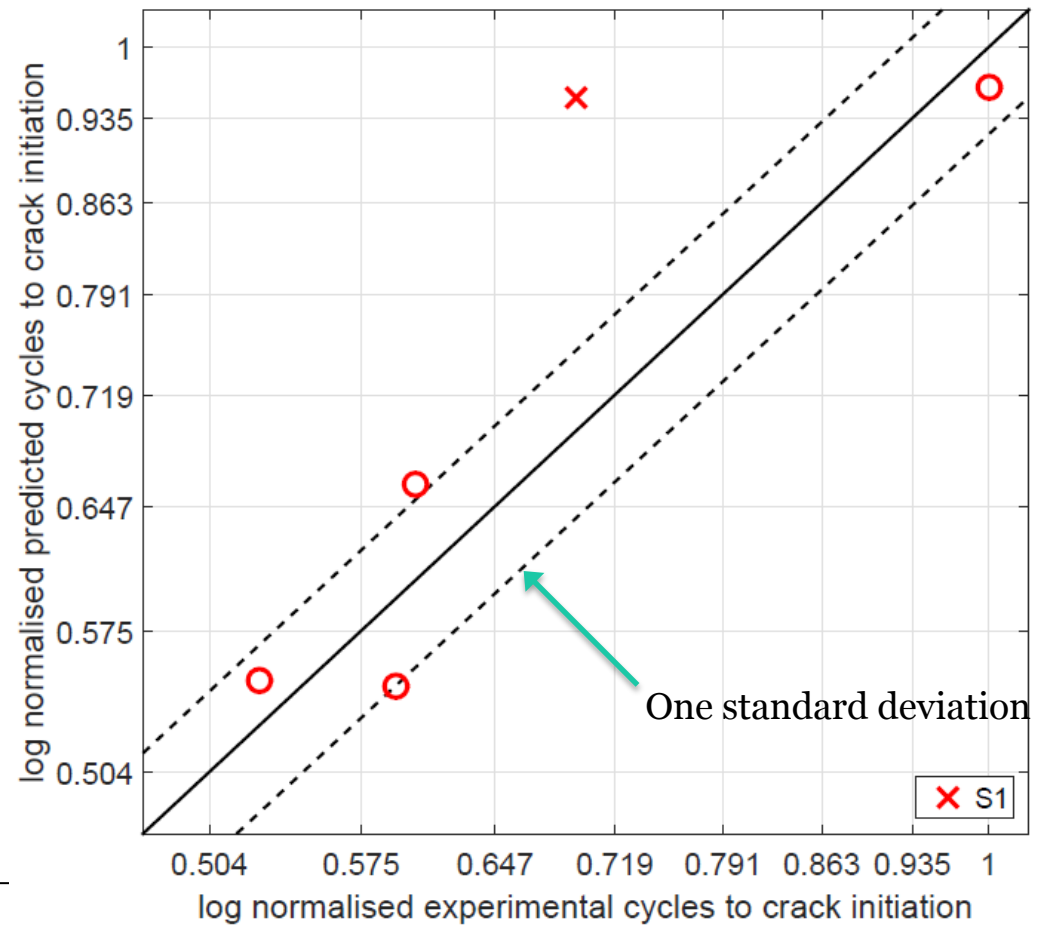
# Experimental lives

- Obtained lives
- How to model this?
- Fatigue damage model:
  - Memory surface
  - Memory stress
  - Plastic strain energy
  - Endurance limit



# Resulting model prediction

- Model fitted to four
- S1: Verification
  - Off by factor 1.37





# Constitutive behaviour

User-defined  
material model

$$f = \sigma_{eq}^{vM} [\hat{\sigma}_{ij} - B_{ij}] - r - \sigma_Y$$

$$\dot{B}_{ij}^k = c_k (a_k \dot{\epsilon}_{ij}^{vp} - B_{ij}^k \lambda), \quad k = 1, 2$$

$$\dot{r}_1 = q_1 \lambda$$

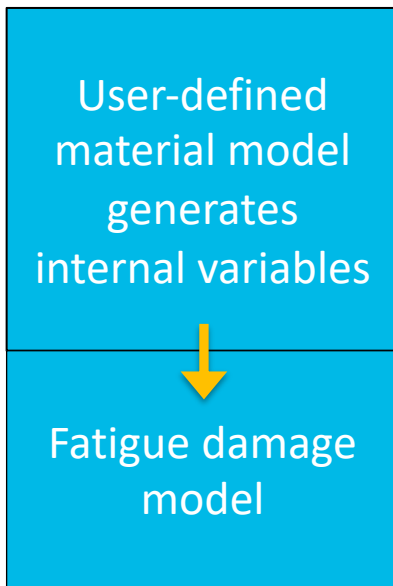
$$\dot{r}_2 = h (q_2 - r_2) \lambda$$

$$\dot{\epsilon}_{ij}^{vp} = \begin{cases} 0 & , f \leq 0 \\ \lambda \frac{\partial f}{\partial \sigma_{ij}} & , f > 0 \end{cases}$$

$$\lambda = \left( \frac{f}{\eta} \right)^m$$

# Crack initiation

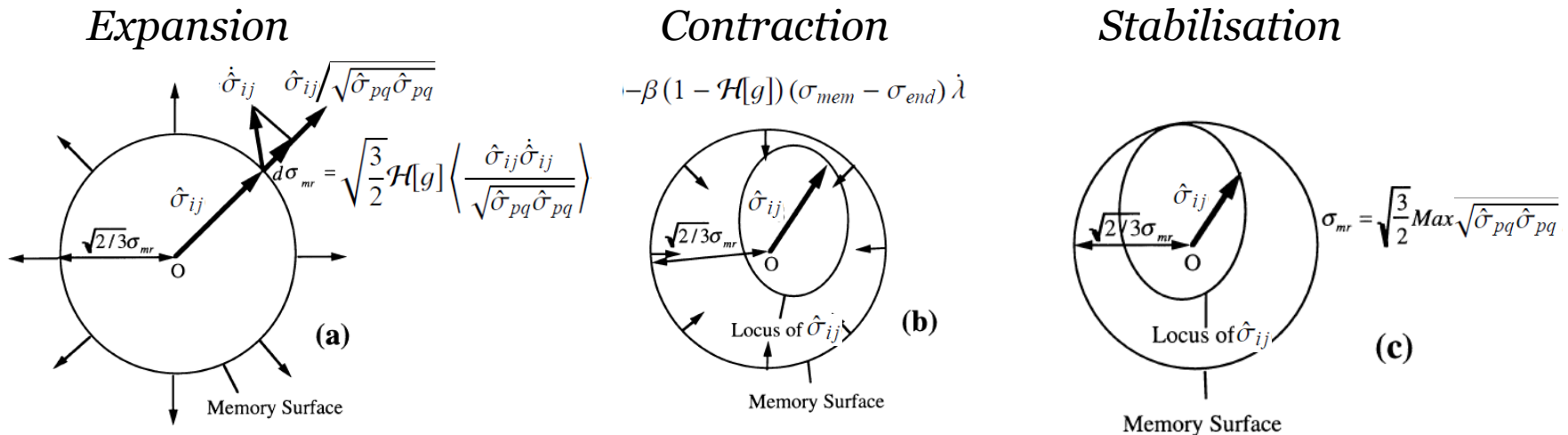
- Add-on to user-defined material model



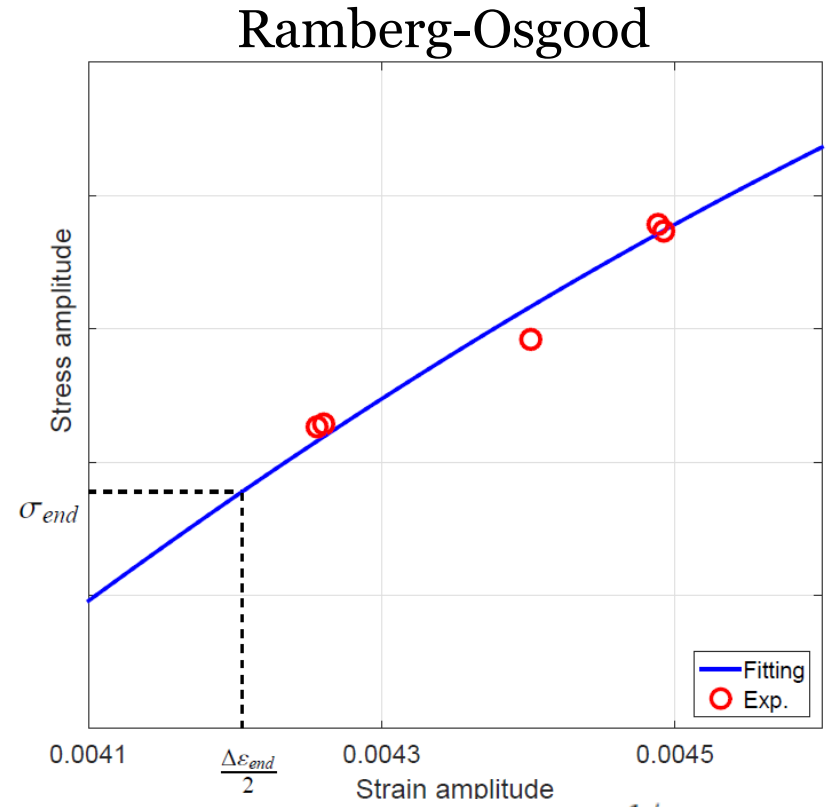
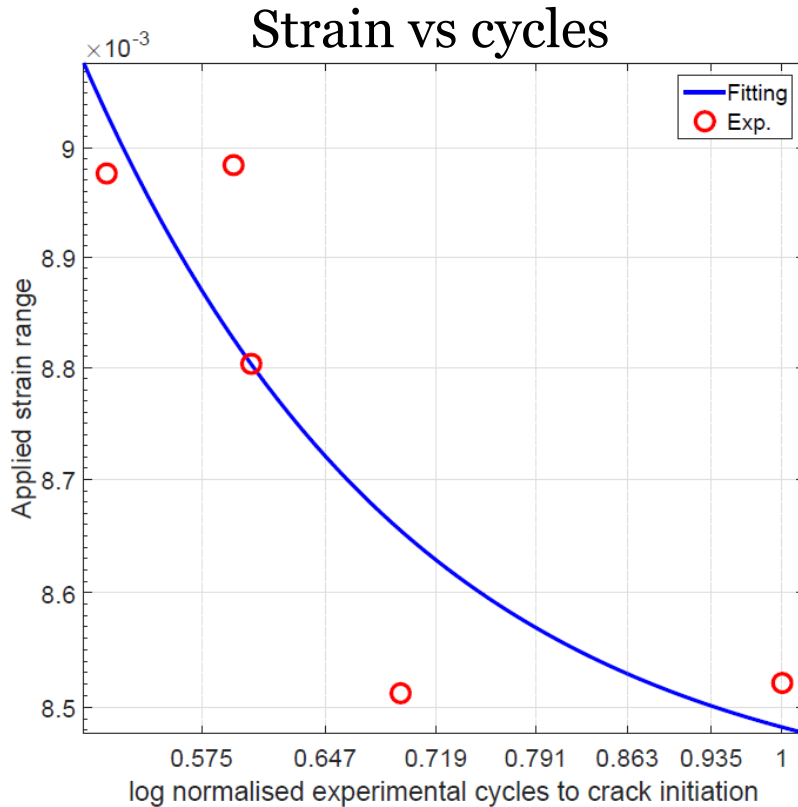
$$\begin{cases}
 g = \sqrt{\hat{\sigma}_{ij}\hat{\sigma}_{ij}} - \sqrt{\frac{2}{3}}\sigma_{mem} \leq 0 \\
 \dot{\sigma}_{mem} = \sqrt{\frac{3}{2}}\mathcal{H}[g] \left\langle \frac{\hat{\sigma}_{ij}\dot{\hat{\sigma}}_{ij}}{\sqrt{\hat{\sigma}_{pq}\hat{\sigma}_{pq}}} \right\rangle - \beta(1 - \mathcal{H}[g])(\sigma_{mem} - \sigma_{end})\dot{\lambda} \\
 \dot{\omega} = \langle \sigma_{mem} - \sigma_{end} \rangle^\alpha \dot{\psi}^p \\
 \dot{\psi}^p = \mathcal{H}[\sigma_{kk}] \sigma_{eq}^{vM} \dot{\lambda}
 \end{cases}$$

# Memory surface

- Analogous to yield surface in plasticity
- Expands with the stress state
- Constant amplitude loading  $\rightarrow \beta = 0$ : no contraction
- Initially  $\sigma_{mem} = \sigma_{end}$



# Fatigue endurance limit



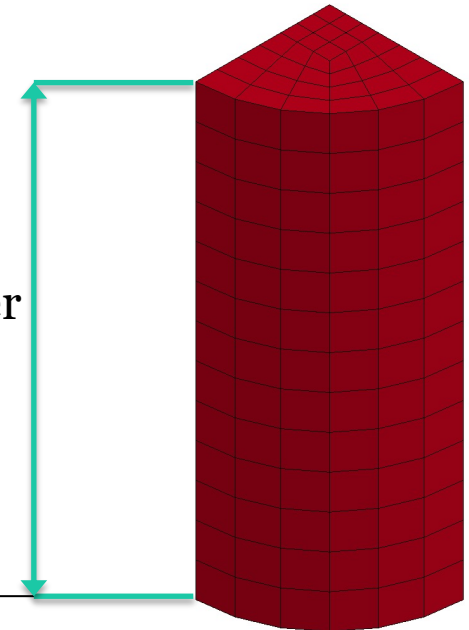
$$(\Delta \epsilon_{mech} - \Delta \epsilon_{end})^d N_i = e$$

$$\frac{\Delta \epsilon}{2} = \frac{\Delta \sigma}{2E} + \left( \frac{\Delta \sigma}{2K} \right)^{1/n}$$

# FE-Simulation

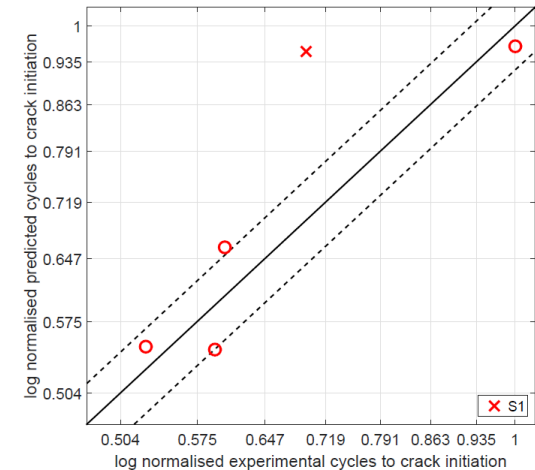
- LS-DYNA – implicit solver
- Quarter model
- Stable state:
  - 5% difference in fatigue damage
  - $\omega_c = \Delta\omega_1 + \dots + \Delta\omega_x + \Delta\omega_{stable}(N_i - x)$
  - ”Cycle jumping”

Extensometer  
gauge length



# Results & Discussion

- Uncertainties – material batches
- Endurance limit coupled to load cycle
- Misguiding due to S1 and S3
- Critical-plane?
- Cycle jumping procedure?



Specimen	Normalised predicted $N_i$	Factor	Experiment Normalised $N_i$	
S1	0.9528	1.3707	0.695	Verification
S2	0.5490	1.0440	0.526	
S3	0.9622	0.9622	1.000	Calibration
S4	0.5459	0.9200	0.593	
S5	0.6610	1.0952	0.604	

# Conclusions

- The constitutive model gave satisfactory response. Difference due to material batches
- Predicts TMF crack initiation within a factor of 1.37 compared to experiments
- Fatigue damage model accounts for load-sequence effects and eliminates cycle-counting methods
- Reduce uncertainties by including more experiments, only four specimens for calibration and one to verify

Thank you!

